

Permanent Magnet Dipoles for the ESRF Upgrade

J. Chavanne, C. Benabderrahmane, C. Penel, G. Le Bec, F. Bidault, M. Paulin, G. Giroud, B. Cottin, E. Fene, P. Arnoux, F. Villar, S. Liuzzo, L. Farvacque, P. Raimondi

OUTLINE

- Context & motivation
- Design
- Construction
- Magnetic measurements
- Temperature stability
- Summary

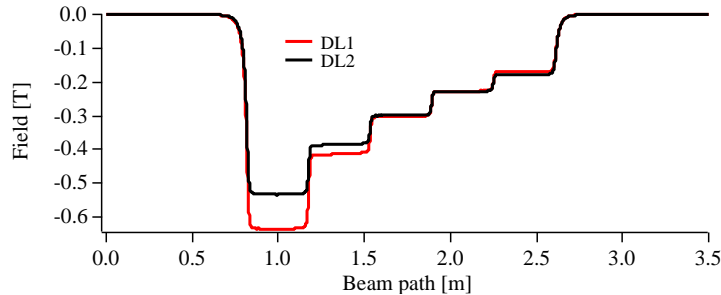


PERMANENT MAGNET DIPOLES

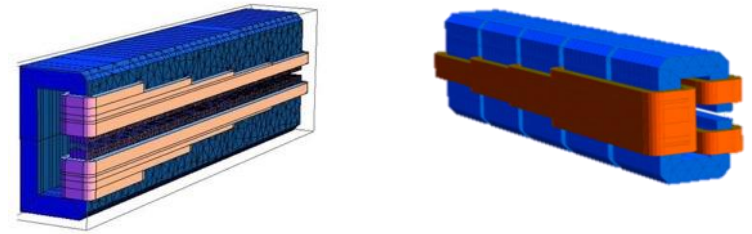
Dipoles with longitudinal gradient (DL)

Non constant field along beam path

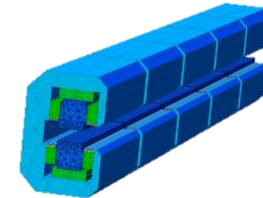
- Field matched to varying horizontal dispersion (emittance reduction)
 - Higher field at lower dispersion
 - Lower field at higher dispersion
- Practically done with field steps (5 in our case)



Early resistive designs



Permanent magnet design

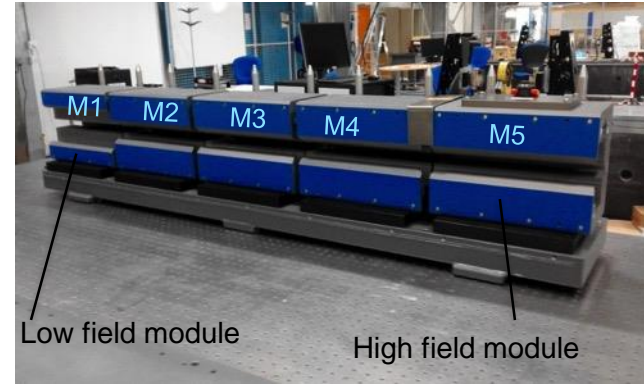


Permanent Magnet (PM) structure

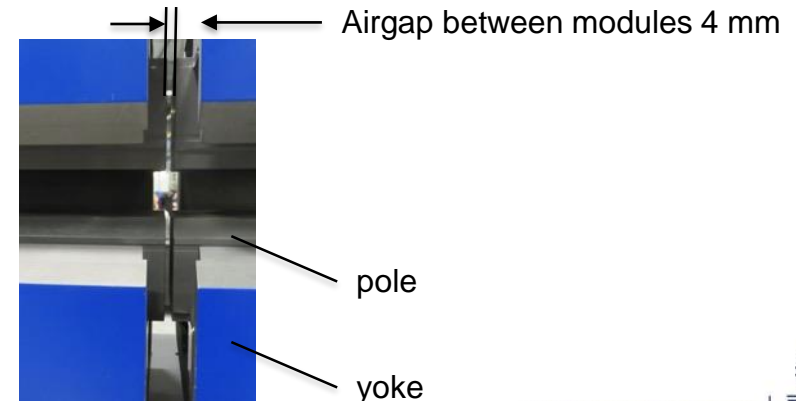
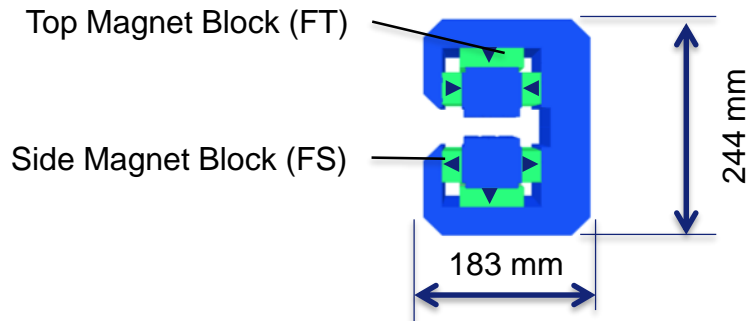
- Demonstrate feasibility of low cost PM Dipoles
 - Low procurement cost
 - Low running cost ~ 0
- Benefits from in-house experience on PM devices (Insertion-Devices)
- Well adapted to the segmentation approach
- compactness

DL MAGNETIC STRUCTURE

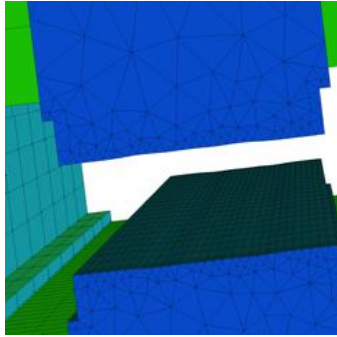
Parameter	Value	Unit
Field	0.64 to 0.17 (DL1) 0.53 to 0.17 (DL2)	T
Mech. length	1784	mm
Gap	25	mm
Deflection angle	31.7 (DL1), 29.4 (DL2)	mrad
Power	0	kW
PM weight/DL	~ 45	kg
# of units	128+4	
GFR (HxV)	26x18	mm
$\Delta B/B$ in GFR	$<10^{-3}$	



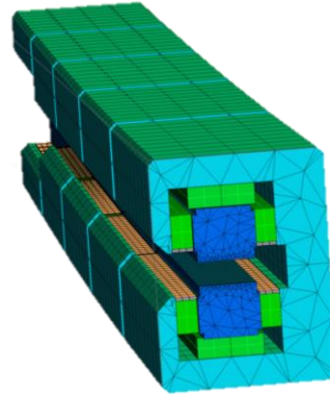
- Module M2 to M5 geometrically identical but populated differently with magnet blocks
- Module M1 (low field) modified for integration of a photon beam absorber



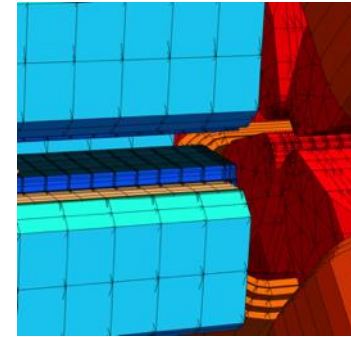
DL MAGNETIC DESIGN



Pole shape optimization



3D magnetic model (RADIA)



Magnetic cross-talk with neighboring magnets



Beam dynamic model

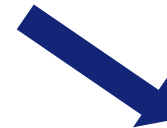
- Field representation
- Magnetic length
- Multipoles
- ..etc



Magnetic optimization

- Magnetic interaction between modules (gap between modules)
- Modules place on curved beam path
- Magnetic crosstalk with neighboring magnet
- Field tuning scheme (flux shunts)
- passive thermal compensation (Fe-Ni shunts)

... etc



Simulation of magnetic measurements (Stretched moving wire)

- individual modules
- full magnet assembly
- Field integrals

PERMANENT MAGNET MATERIAL

PM material: $\text{Sm}_2\text{CO}_{17}$ XGS30H (Magsound, China, <http://www.magsound.com>)



Recent progress in $\text{Sm}_2\text{CO}_{17}$ materials @ Magsound

Material	Grade	Energy Product(BH)max		Residual Induction Br		Coercive Force HcB		Intrinsic Coercive Force Hcj		Density D g/cm ³	Rev.Temp Coeff α(Br) %/°C	Curie Temp TC °C	Max Working Temp Tw °C
		KJ/m ³	MGsOe	T	KGs	KA/m	KOe	KA/m	KOe				
New grades	XGS30M	223-247	28-31	1.08-1.12	10.8-11.2	318-804	4.0-10.1	398-1194	5.0-15.0	8.4	-0.03	≥850	350
	XGS30	223-247	28-31	1.08-1.12	10.8-11.2	700-828	8.8-10.4	1194-1990	15.0-25.0				
	XGS30H	223-247	28-31	1.08-1.12	10.8-11.2	700-828	8.8-10.4	≥1990	≥25.0				
	XGS32M	231-255	29-32	1.10-1.15	11.0-11.5	318-804	4.0-10.1	398-1194	5.0-15.0				
	XGS32	231-255	29-32	1.10-1.15	11.0-11.5	755-850	9.5-10.7	1194-1990	15.0-25.0				
	XGS32H	231-255	29-32	1.10-1.15	11.0-11.5	755-858	9.5-10.8	≥1990	≥25.0				
	XGS33M	238-255	29.9-32	1.12-1.17	11.2-11.7	318-836	4.0-10.5	398-1194	5.0-15.0				
	XGS33	238-255	29.9-32	1.12-1.17	11.2-11.7	820-860	10.3-10.8	1194-1990	15.0-25.0				
	XGS33H	238-255	29.9-32	1.12-1.17	11.2-11.7	843-868	10.6-10.9	≥1990	≥25.0				

15000 magnet blocks ordered (~13000 effectively used)

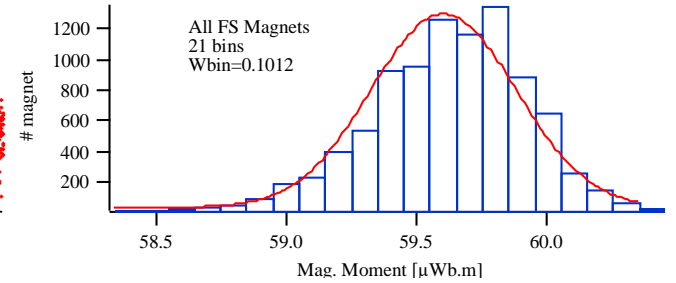
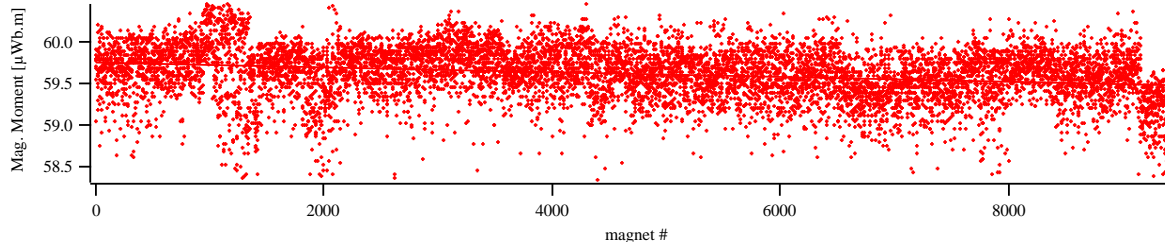
- 6 tons of material
- 2 main types of PM blocks + 1 for field adjustment (¼ block)
- Two batches: delivery September 2016 & December 2016
- Thermal stabilization @ 120 C

$\text{Sm}_2\text{CO}_{17}$

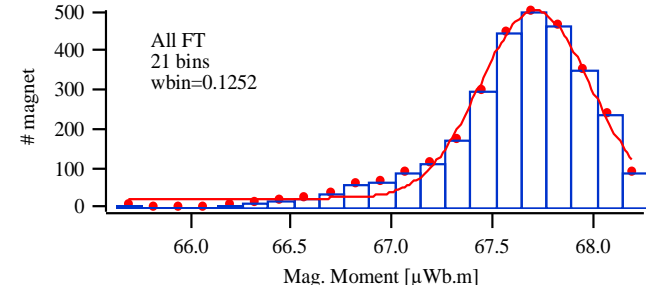
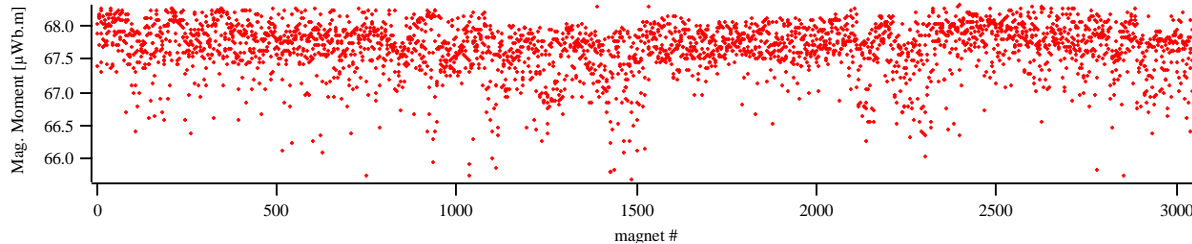
- Low temperature coefficients
- High radiation hardness
- Resistance to radiation induced demagnetization

MAGNET BLOCKS DATA

Measured magnetic moments



Magnet type FS: $(\text{max-min})/\text{avg}=3.5\%$, $\text{stdev}/\text{avg}=0.52\%$



Magnet type FT: $(\text{max-min})/\text{avg}=3.9\%$, $\text{stdev}/\text{avg}=0.57\%$

Use of magnet sorting

DL IRON MATERIAL: CONTROL OF STEEL QUALITY

Raw hot rolled material (low carbon steel)



Flame cutting + heat treatment



Semi finished product (iron blocks)



Delivery to sub-contractors for machining
Surface treatment
Assembly without PM
Painting

DL ASSEMBLY: DONE IN-HOUSE

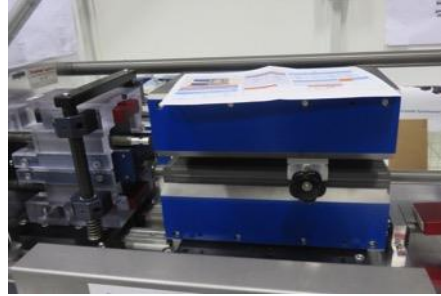
Magnet blocks (Magsound,)



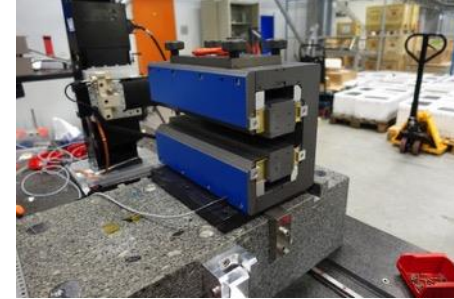
Machined empty modules
AMF (UK), CECOM (It)



Magnet block insertion in modules
(dedicated tools)



Magnetic measurement & field tuning
for individual modules
(stretched wire)



DL assembly



Magnetic measurements of full DL & final field tuning
(stretched wire)

DL FOR LATTICE DESCRIPTION

Example DL2 model with 5 (field, magnetic length)

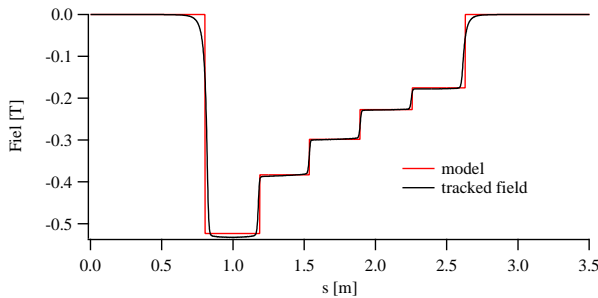
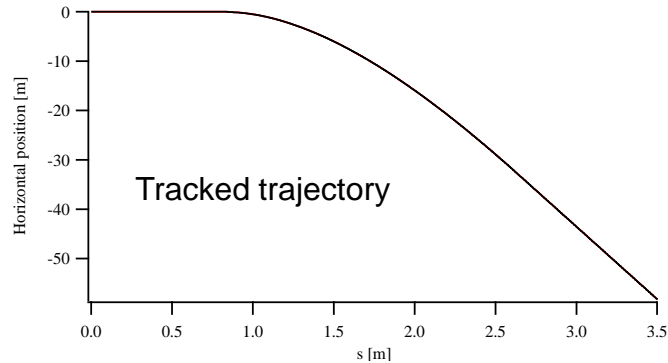
Find $B_i, L_i (i = 1,5)$

with

$$\sum_{i=1}^5 B_i L_i = \textit{nominal integral}$$

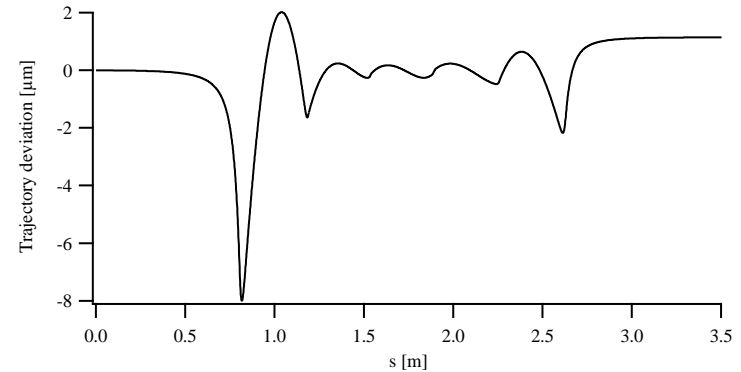
and

$\textit{Min} (|\textit{modelled trajectory} - \textit{tracked trajectory}|)$



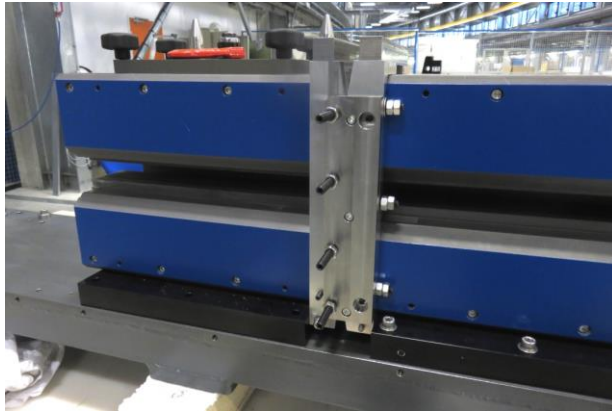
DL2

B [T]	L[m]
-0.5232	0.383
-0.3831	0.348
-0.2979	0.356
-0.2273	0.365
-0.1751	0.371



MODULAR CONCEPT

5 independent modules/ DL

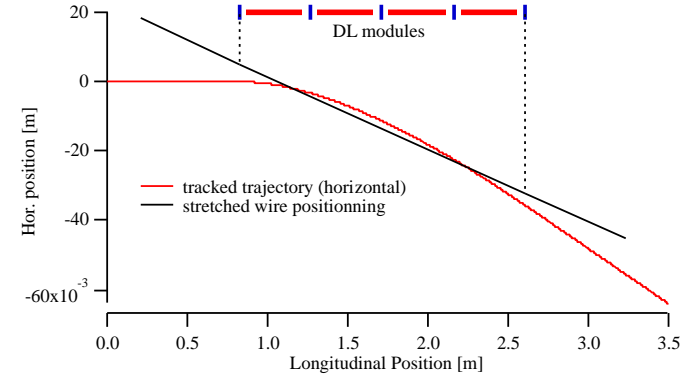
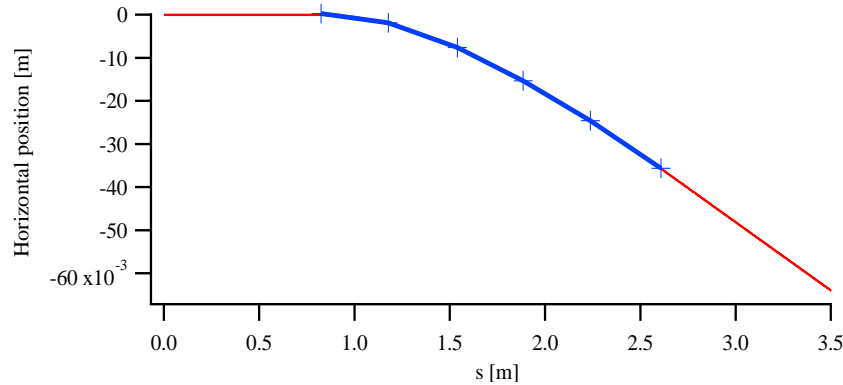


A module can be removed/installed from/in the assembly
Possible implementation of quadrupole function in one or two modules

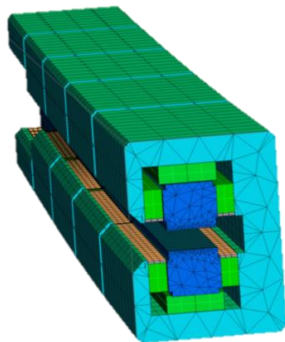
- Same yoke
- Modified pole & magnet block distribution
- Future development

ANTICIPATION OF MAGNETIC MEASUREMENTS WITH 3D MODEL

Stretched wire positioned according to the best line fit of tracked trajectory between end pole faces of DL



Module axis placed on trajectory (5 straight segments)



~ curved magnet



- Field tuning of each module
 - Limited tuning of the full assembly
 - Needs knowledge of the “ideal” integral for each module
 - Tuning done with Fe-Si shims (flux shunt)



Needs to anticipate the magnetic crosstalk between modules to achieve targeted DL integral:

$$\left| I_{sum} = \sum_{k=1}^5 I_k \right| > |I_{DL}|$$

Integral of individual module

Integral of full assembly

Movable flux shunt

Fe-Si shims

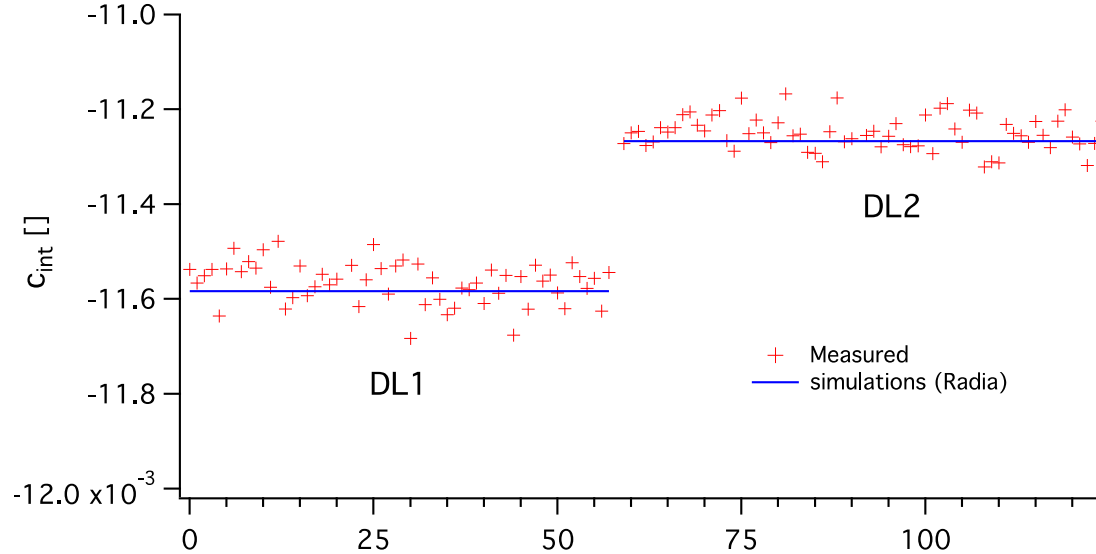


Simulation results

$$c_{int} = \frac{I_{sum} - I_{DL}}{I_{DL}} = \begin{cases} -1.13 \% \text{ for DL2} \\ -1.16 \% \text{ for DL1} \end{cases}$$

MAGNETIC CROSSTALK BETWEEN MODULES

Magnetic measurements of individual modules and assembly give access to c_{int}



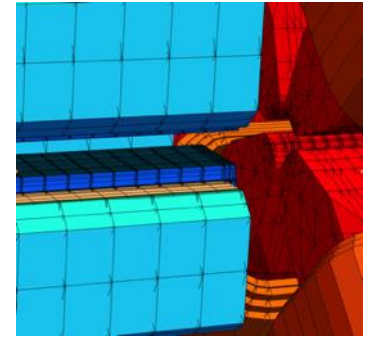
$$c_{int} = \frac{I_{sum} - I_{DL}}{I_{DL}}$$

The measured values for c_{int} agree very well with simulations

MAGNETIC CROSSTALK WITH NEIGHBORING QUADRUPOLES

distance iron to iron quadrupole DL

- 47 mm for DL1 (both sides)
- 47 mm & 150 mm for DL2

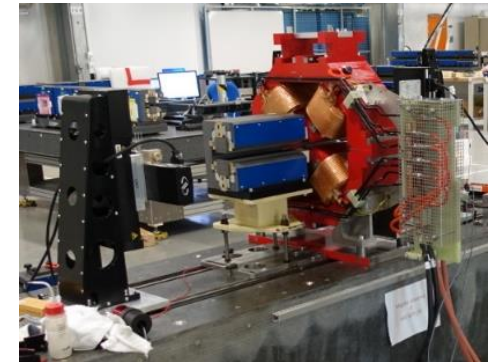


Magnetic simulation :

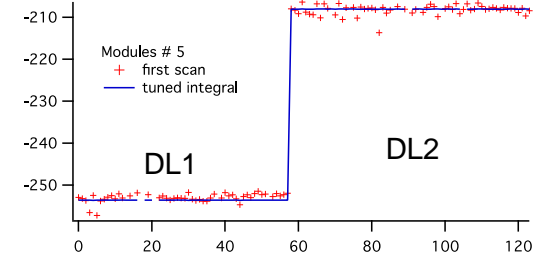
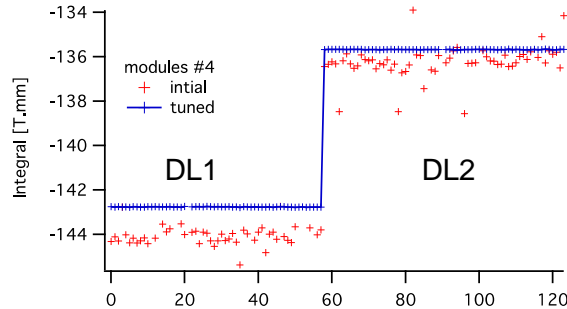
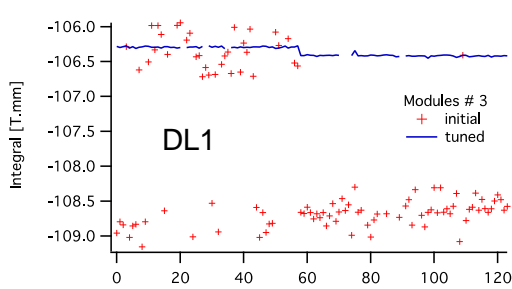
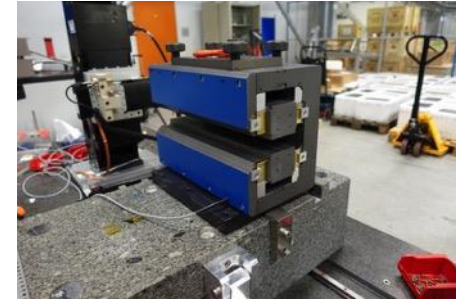
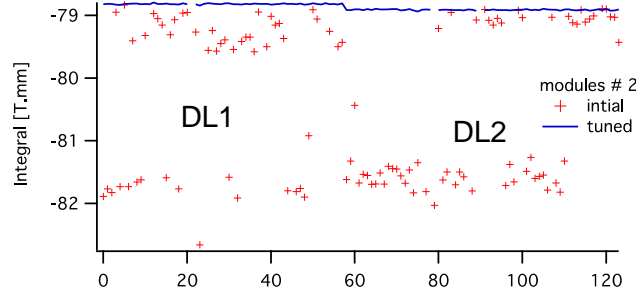
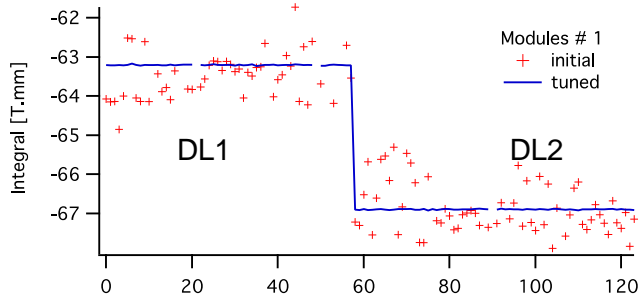
- 0.46 % reduction in deflection angle for DL1
- 0.15 % for DL2
- Confirmed with measurements

End module strength increased by 0.96 % for DL1

End module strength increased by 0.96 % & 0.13% for DL2



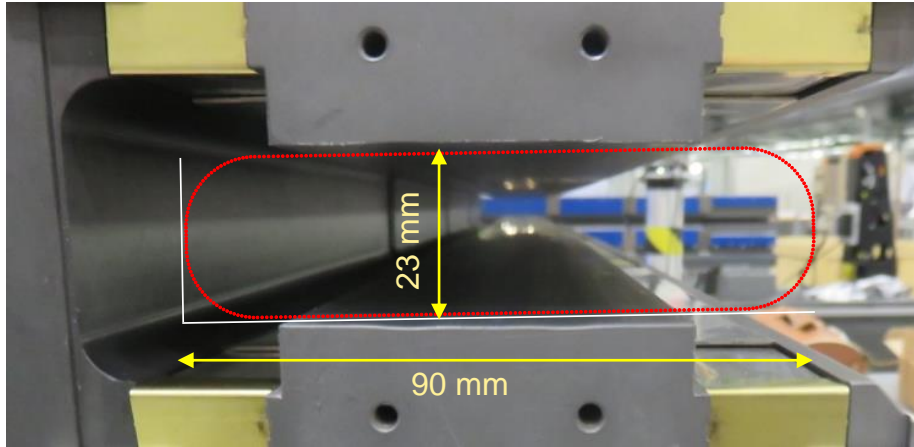
MEASUREMENT AND TUNING OF INDIVIDUAL MODULES



In total 132 x 5 modules assembled and tuned

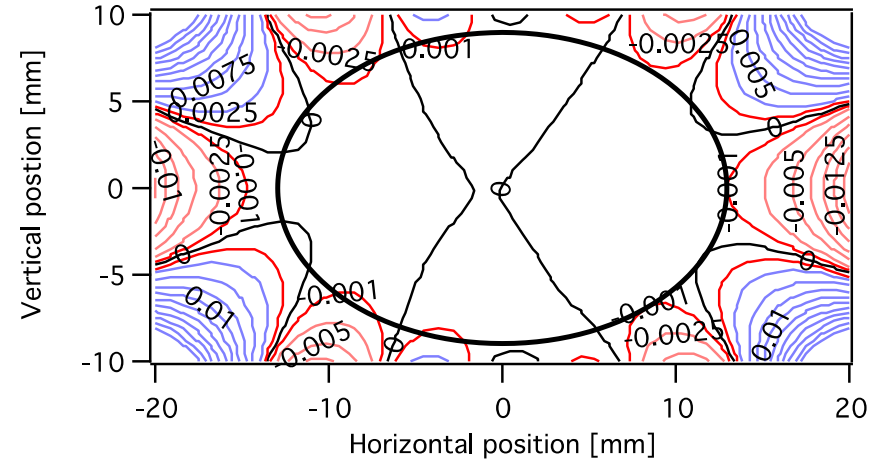
DL MAGNETIC MEASUREMENTS

DLs

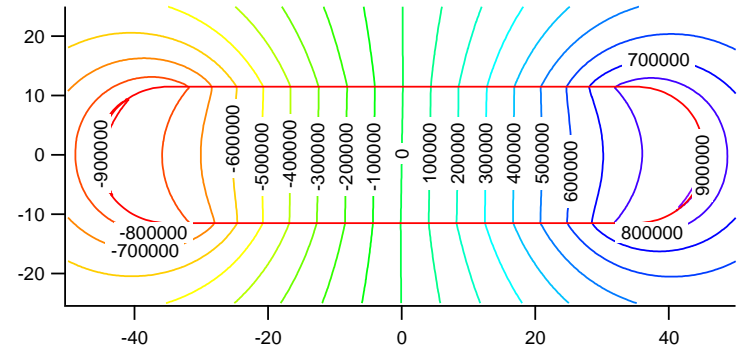


- 332 segments
- pole gap 24.5 mm
- Segment length 0.62 mm

DB/B

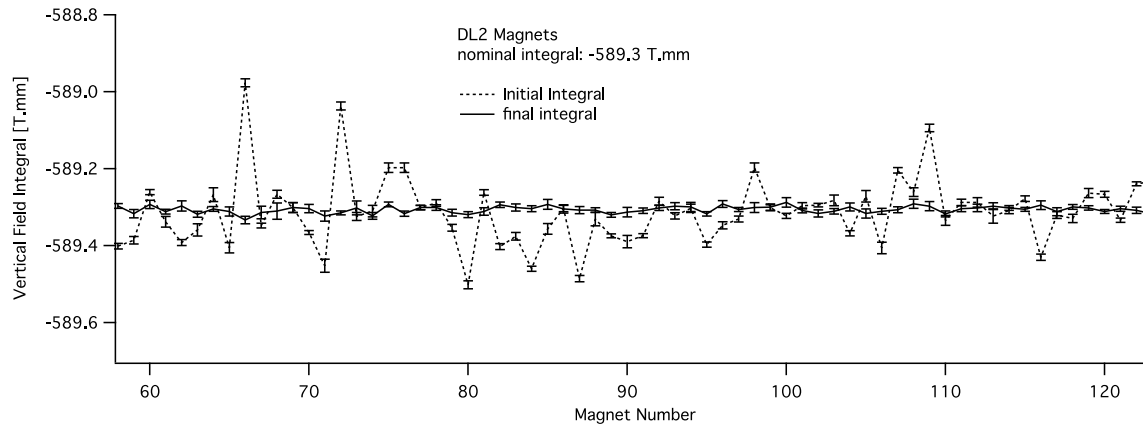
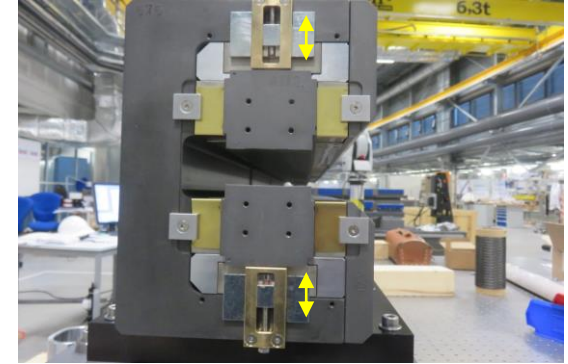
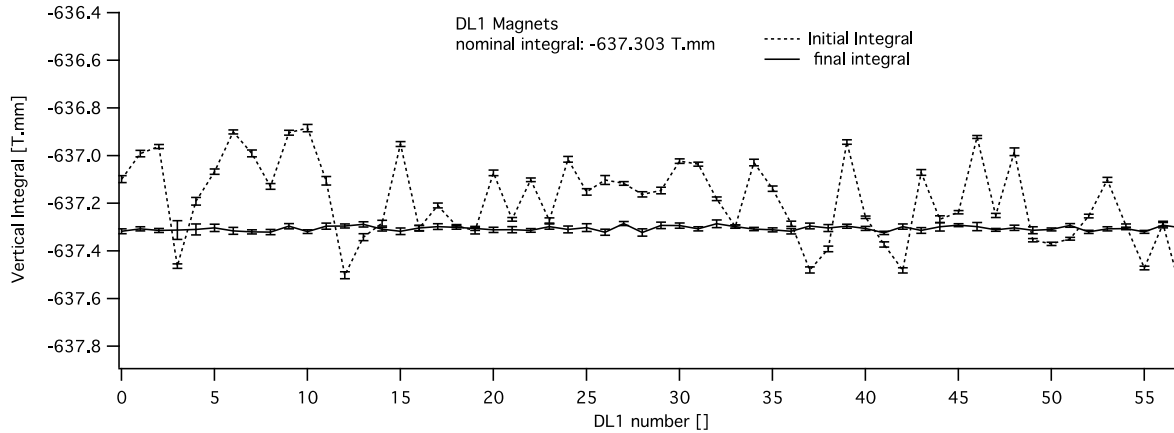


Field integral homogeneity in GFR



DL FIELD INTEGRAL AT CENTER

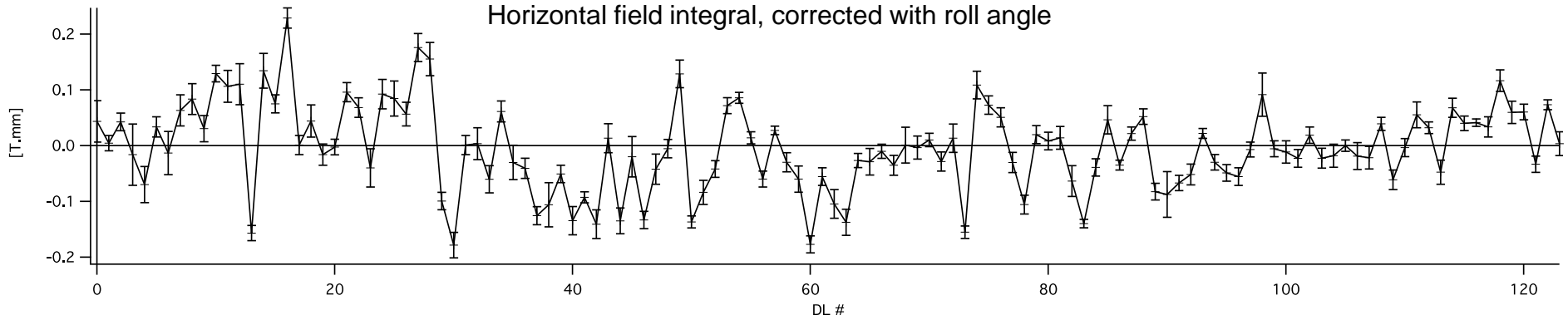
DL field tuning using movable shunts



Measurement repeatability

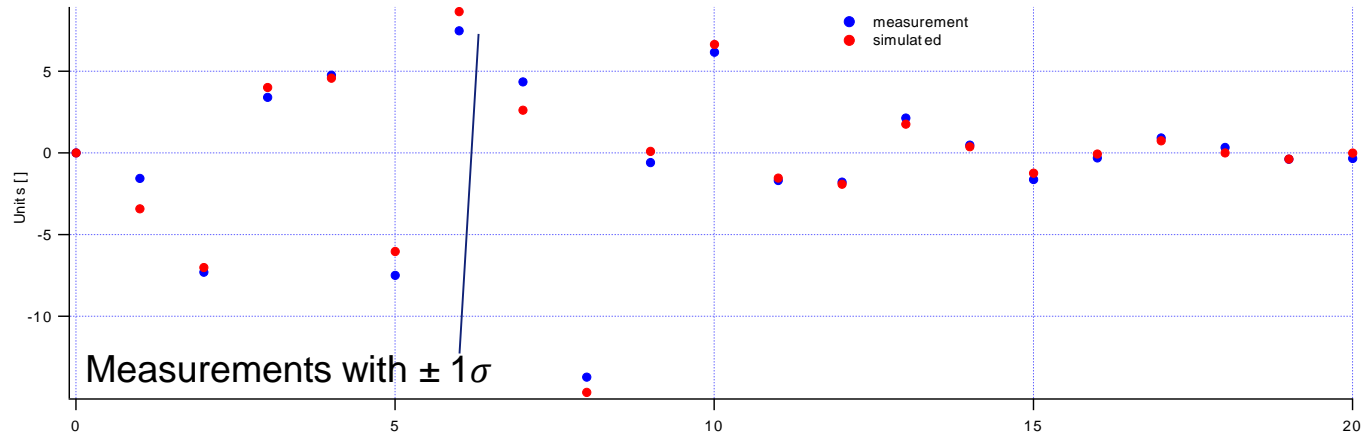
$$1\sigma/B \approx 2.510^{-5}$$

FIELD INTEGRAL & HARMONIC ANALYSIS (STRAIGHT INTEGRALS)

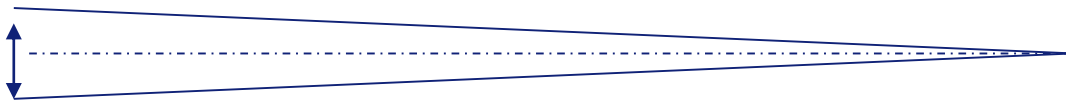
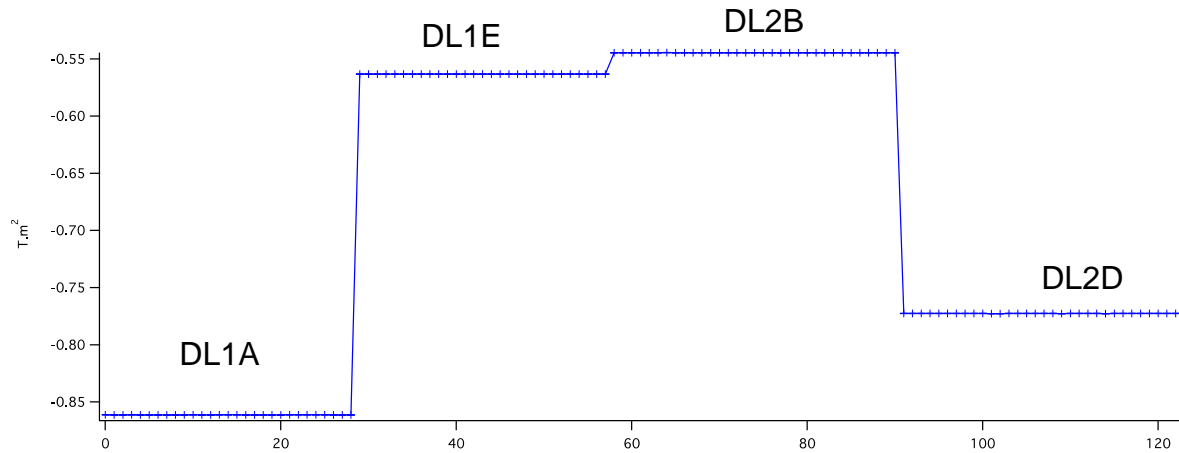


Harmonic analysis

Simulation using RADIA model



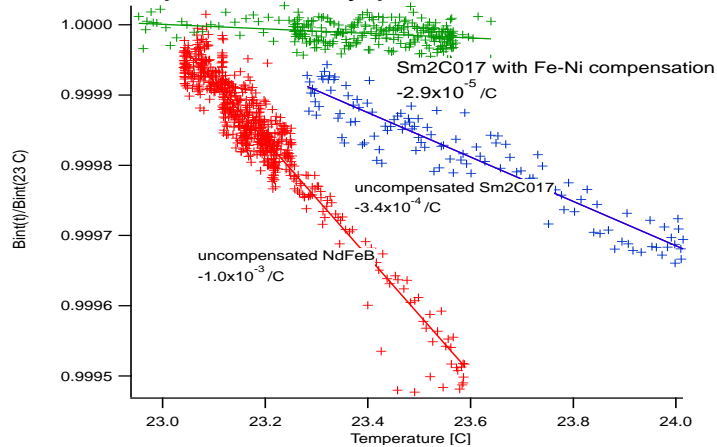
2ND INTEGRAL



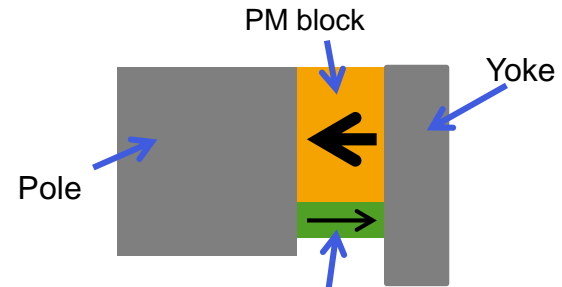
Second integral tuned with movable end shims.

TEMPERATURE STABILITY

- Dominated by PM material temperature coefficient
- Can be compensated by passive FeNi shunts

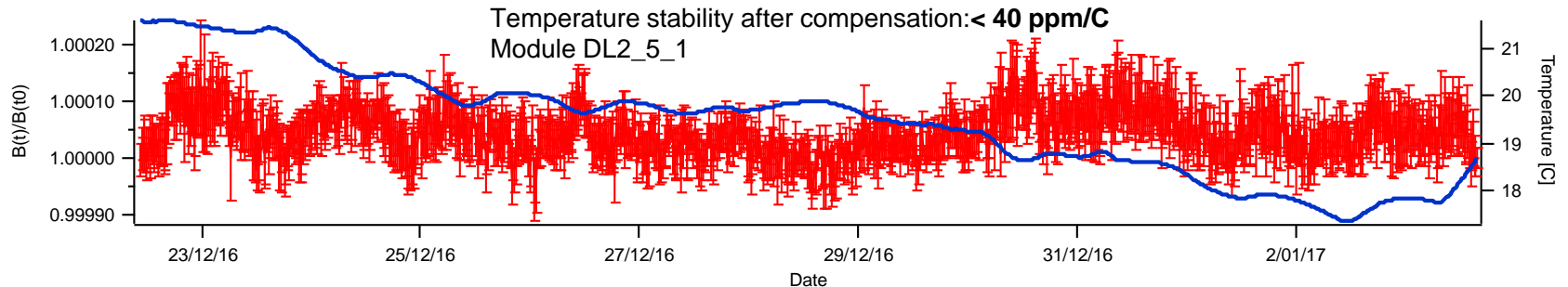


Material	$C_T = dB/B/dT$
$\text{Sm}_2\text{Co}_{17}$	$-3.3 \cdot 10^{-4}$
$\text{Nd}_2\text{Fe}_{14}\text{B}$	-10^{-3}

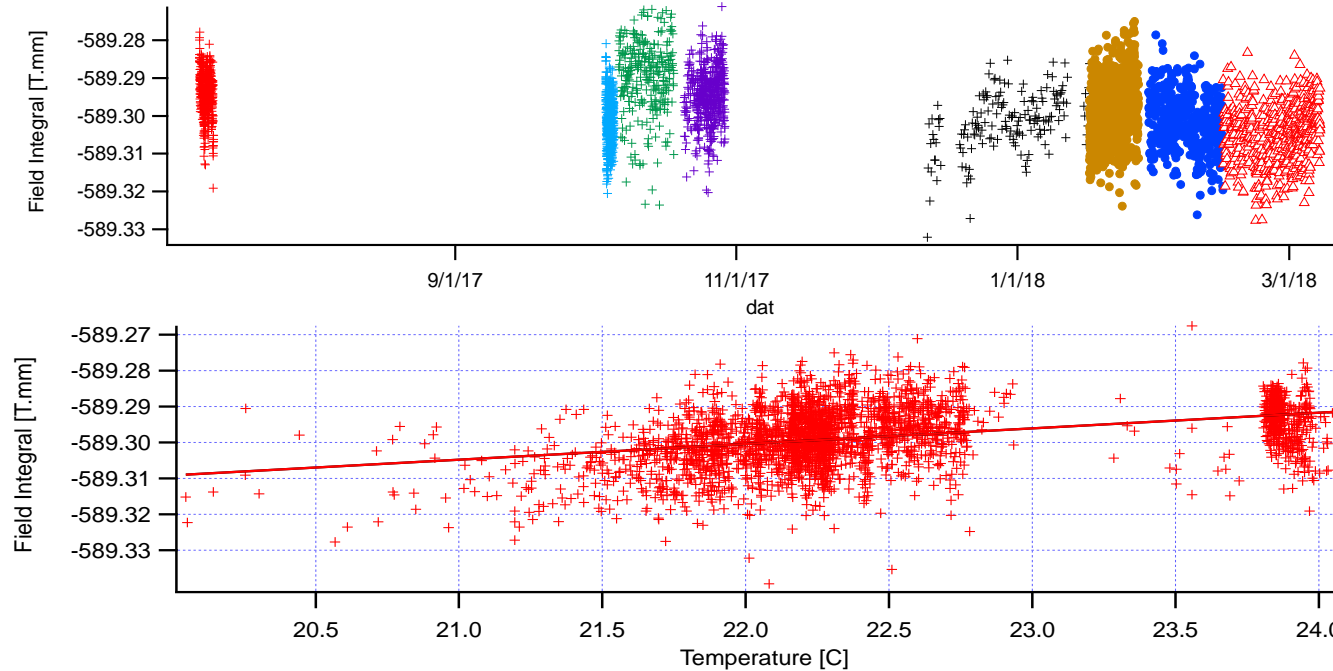


Field integral measurements on PM DL modules NdFeB, $\text{Sm}_2\text{Co}_{17}$

Special FeNi shunt, thickness 0.8 mm to 4.5 mm depending on module type (Thermoflux 55/100 G, curie temperature ~ 55 C, ~ -2%/C)



Measurement of integral & temperature vs time



Residual slope ~ 10 ppm/C

Magnet: DL2B_11_14

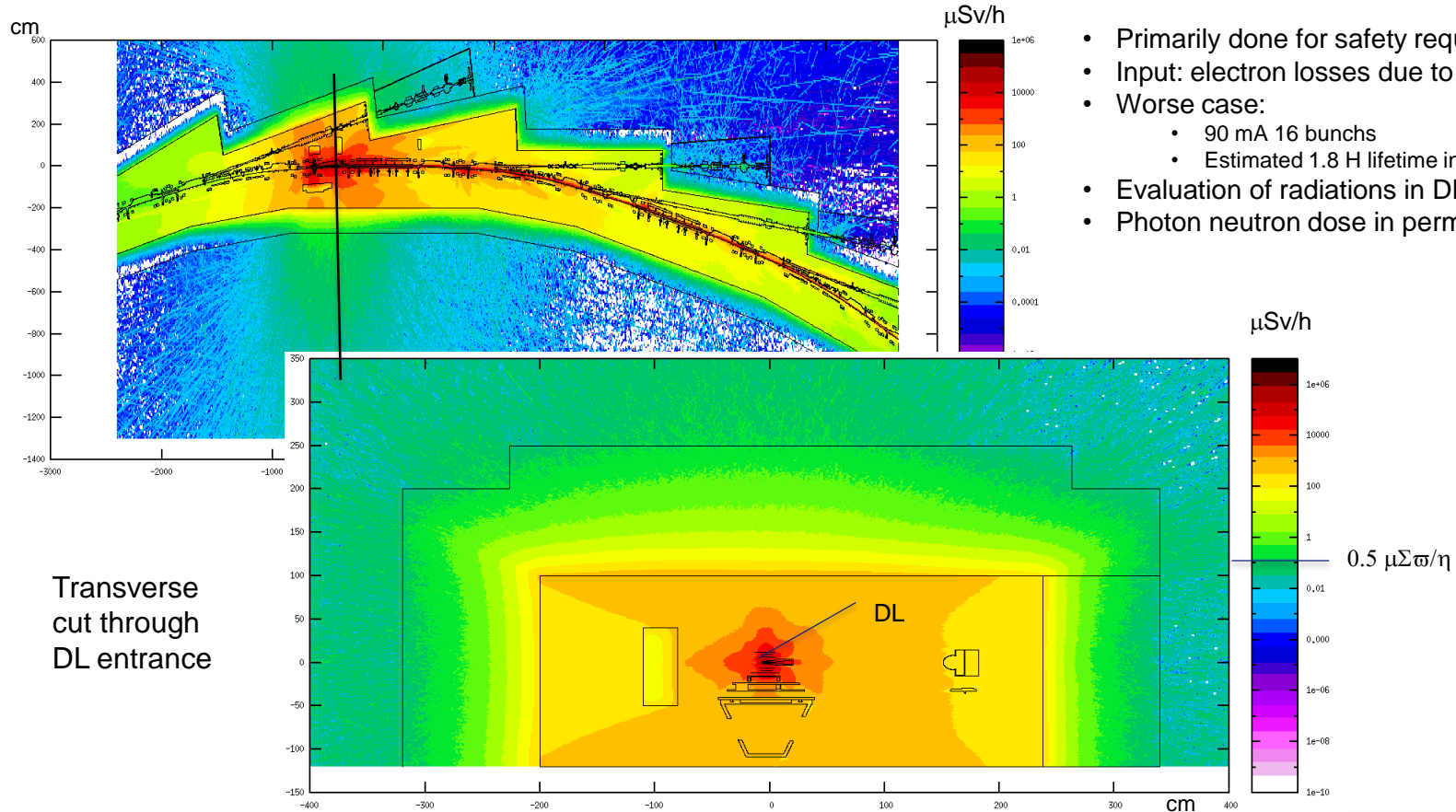
RADIATIONS IN PERMANENT MAGNETS

ESRF storage ring: 6 GeV,

Critical place is at the DL behind the electron beam collimator

FLUKA simulations

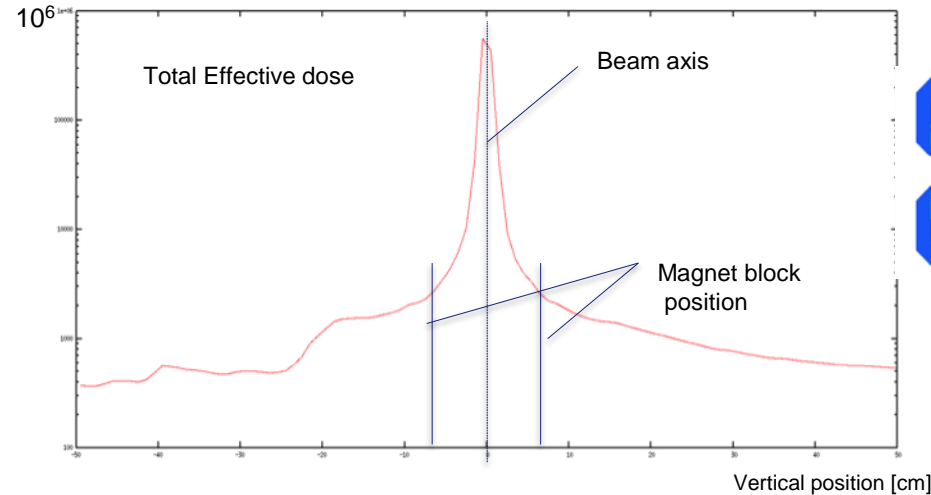
- Primarily done for safety requirements
- Input: electron losses due to Touschek effect
- Worse case:
 - 90 mA 16 bunches
 - Estimated 1.8 H lifetime in EBS
- Evaluation of radiations in DL
- Photon neutron dose in permanent magnets



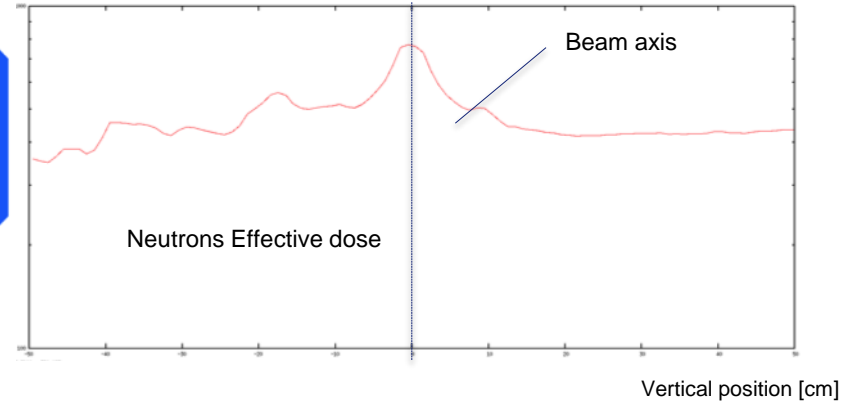
Transverse
cut through
DL entrance

RADIATIONS IN PERMANENT MAGNETS (CONT'D)

mSv/h Vertical dose line profile averaged over 15 mm horizontally



mSv/h
 10^3



In present storage ring $\text{Sm}_2\text{CO}_{17}$ permanent magnets used in low gap undulators: In-Vacuum undulators

- Magnetic gap 6 mm
- Neutron doses at PM blocks are ~ 1 Gy/h derived from beam loss measurements
- No visible demagnetization of permanent magnet material after 15 years of operation ($< 0.2\%$)

Magnetic stability vs radiations should be enough for 20-25 years operation

Status

- Production completed before mid October 2017
- Installed in the ring tunnel



Summary

- Methods and technics for a large scale production of PM dipoles have been developed
- Simple magnetic structures, no electrical power
- Segmented (modules) approach for DLs has interesting flexibility
- $\text{Sm}_2\text{Co}_{17}$ material is the most suitable to ensure long term magnetic stability
- Magnetic measurements with stretched moving wire very efficient and reliable