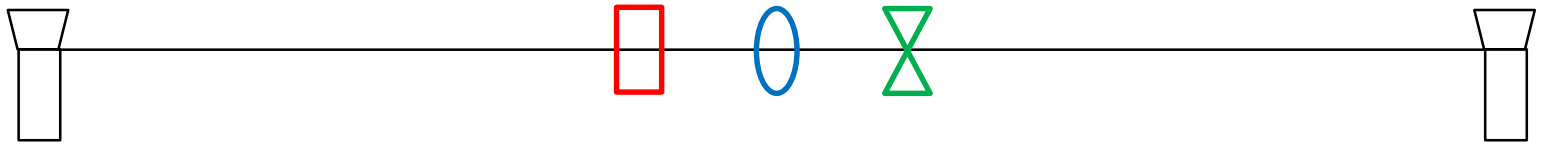


International Magnetic Measurement Workshop 21
ESRF, Grenoble, FR, June 2019

A stretched wire system for
the measurement of accelerator lattice and
insertion device magnets



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Contents

- Motivation
- Analysis Method and Simulation Results
- Stretched wire measurement system
- Experimental results
 - A Quadrupole Magnet
 - In-vacuum Undulator
 - Circular path
 - Elliptical path
- Conclusions

Introduction

TLS: Taiwan Light Source (1993-now)

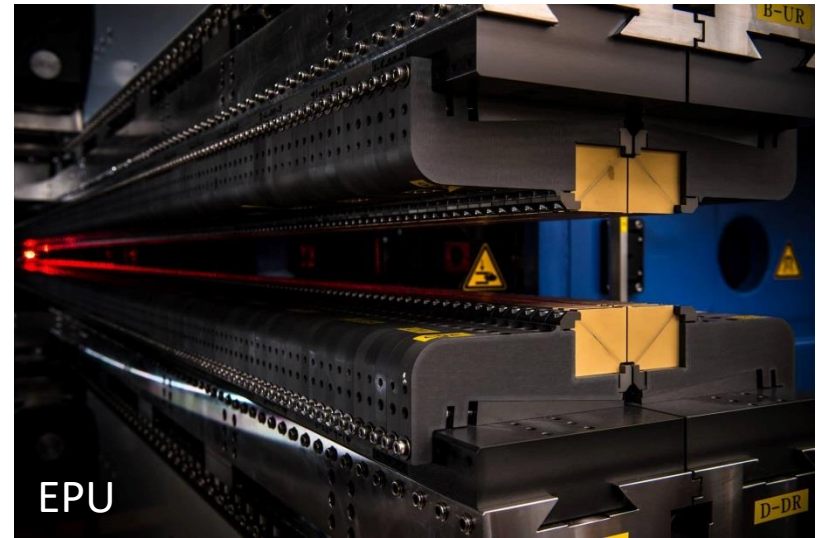
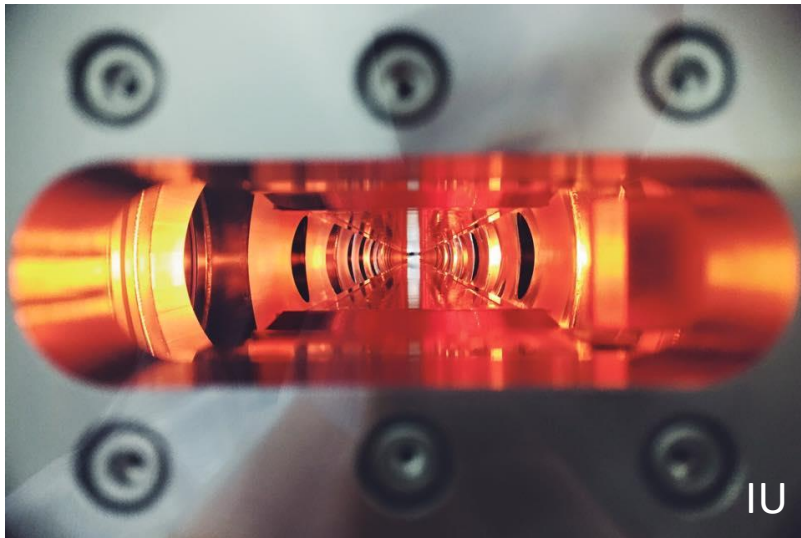
TPS: Taiwan Photon Source (2015-now)



- 2014** Aug. Booster ring and storage ring accelerators installed
- Dec. The first TPS light at the 3-GeV design beam energy delivered.
- 2015** Jan. Taiwan Photon Source Inauguration Ceremony.
- Dec. TPS exceeds its design beam current 500 mA
- 2016** Sep. TPS Opening Ceremony.
Four TPS phase-I beamlines available to users worldwide.
- 2017** May. Flagship Project initiated – construction of 5 TPS phase-II beamlines begins
- Dec. Construction of TPS phase-I beamlines completed

Motivation

- Small bore measurement for ultimate storage ring.
- Elliptical measurement for closed aperture of dipole and insertion device.



Analytic Methods

The magnetic field $B_y + iB_x$ is expressed in polynomial expansions as

$$B_y + iB_x = \sum (b_n + ia_n)(x + iy)^n \quad (1)$$

The equation is divided into real part B_y and imaginary part B_x

$$B_y(x, y) = b_0 + a_1 y + b_1 x + 2a_2 xy + b_2(x^2 - y^2) + \dots \quad (2)$$

$$B_x(x, y) = a_0 + a_1 x - b_1 y - 2b_2 xy + a_2(x^2 - y^2) + \dots \quad (3)$$

b_0 : normal dipole term

b_1 : normal quadrupole term

a_0 : skew dipole term

a_1 : skew quadrupole term

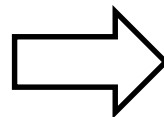
Polynomial fit

Data

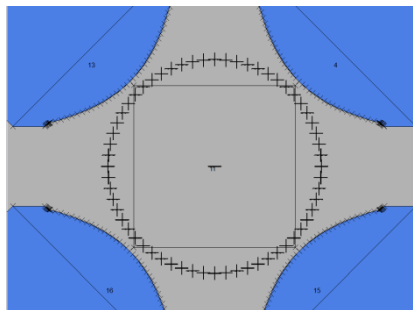
Format

X_1, Y_1, B_{y1}
 X_2, Y_2, B_{y2}
 X_3, Y_3, B_{y3}
 \cdot
 \cdot
 \cdot
 X_j, Y_j, B_{yj}

Choose fitting number n



$$B_y(x, y) = b_0 + a_1y + b_1x + 2a_2xy + b_2(x^2 - y^2) + \dots$$



A circle path divided to j points

X_1, Y_1, B_{x1}
 X_2, Y_2, B_{x2}
 X_3, Y_3, B_{x3}
 \cdot
 \cdot
 \cdot
 X_j, Y_j, B_{xj}

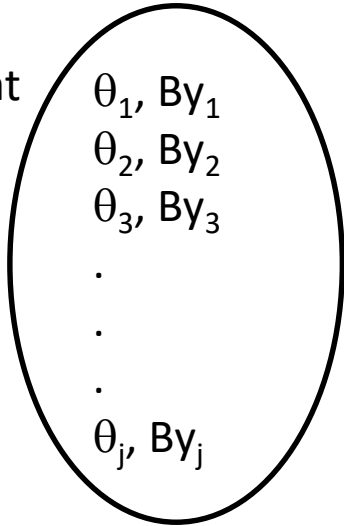
$$B_x(x, y) = a_0 + a_1x - b_1y - 2b_2xy + a_2(x^2 - y^2) + \dots$$

b_0, a_0
 b_1, a_1
 b_2, a_2
 b_3, a_3
 \cdot
 \cdot
 \cdot
 b_n, a_n

b_0, a_0
 b_1, a_1
 b_2, a_2
 b_3, a_3
 \cdot
 \cdot
 \cdot
 b_n, a_n

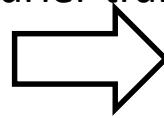
FFT

Data
Format

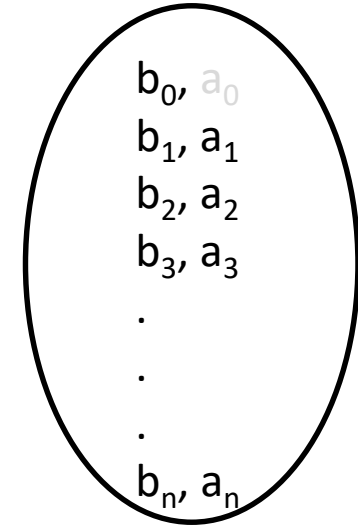


$$By+iBx=\Sigma(b_n+ia_n)r^n e^{in\theta}$$
$$By(\theta)=\Sigma r^n [b_n \cos(n\theta)-a_n \sin(n\theta)]$$

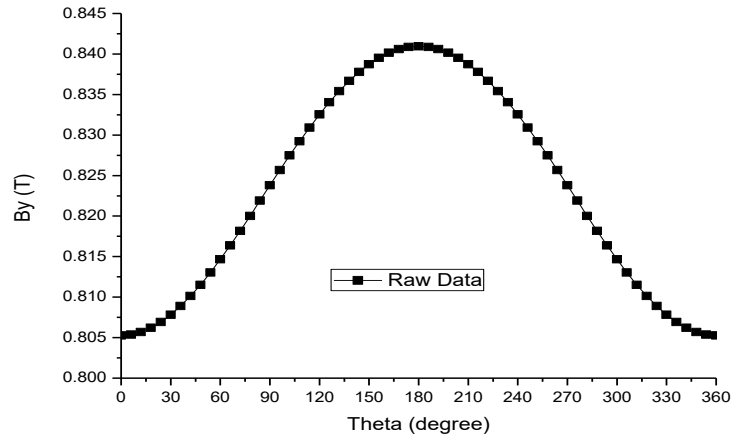
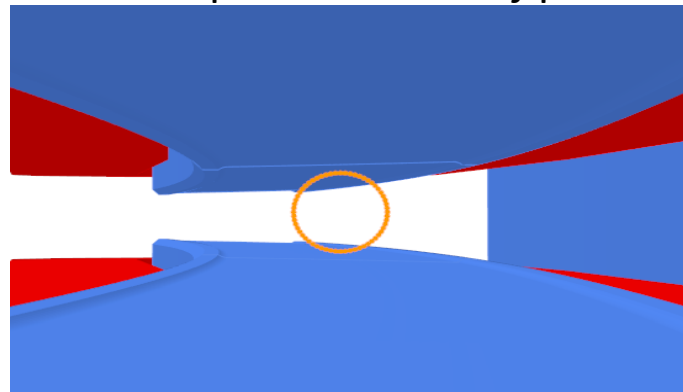
Fast Fourier transfer



j points can define n number



A circle path divided to j points



Pierre Schnizer

P.Schnizer et al. "Theory and Application of Plane Elliptic multipoles for Static Magnetic Fields", NIMA 607(3):505-516, 2009

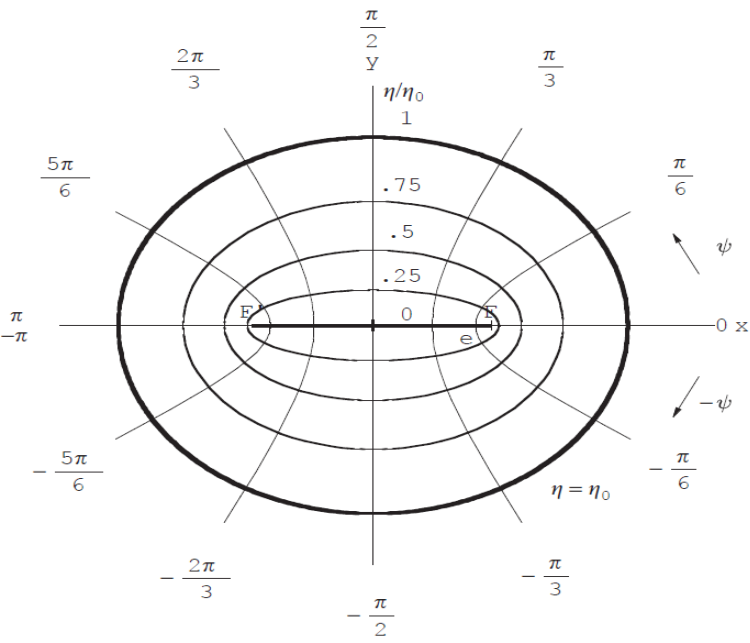


Fig. 1. Plane elliptic coordinates η, ψ , Foci F, F' are at $x = \pm e$.

$$\begin{aligned} x &= e \cosh \eta \cos \psi, & 0 \leq \eta < \infty \\ y &= e \sinh \eta \sin \psi, & -\pi \leq \psi \leq \pi. \end{aligned} \quad (13)$$

$$\mathbf{B}(\mathbf{z}) := B_y + iB_x$$

$$\mathbf{B}(\mathbf{z})/\mathcal{B}_0 = \sum_{m=0}^{\infty} \mathbf{C}_m \left(\frac{r}{R}\right)^m e^{im\theta} = \sum_{m=0}^{\infty} \mathbf{C}_m \left(\frac{x+iy}{R}\right)^m. \quad (8)$$

$$\mathbf{C}_m = \frac{1}{2\pi} \int_{-\pi}^{\pi} \frac{\mathbf{B}_0(\theta)}{\mathcal{B}_0} e^{-im\theta} d\theta. \quad (9)$$

Circular multipoles

$$\mathbf{B}/\mathcal{B}_0 = \frac{\mathbf{E}_0}{2} + \sum_{n=1}^{\infty} \mathbf{E}_n \frac{\cosh[n(\eta + i\psi)]}{\cosh(n\eta_0)}. \quad (24)$$

$$\mathbf{E}_n = \frac{1}{\pi \mathcal{B}_0} \int_{-\pi}^{\pi} \mathbf{B}_0(\mathbf{z} = e \cosh(\eta_0 + i\psi)) \cos(n\psi) d\psi \quad (27)$$

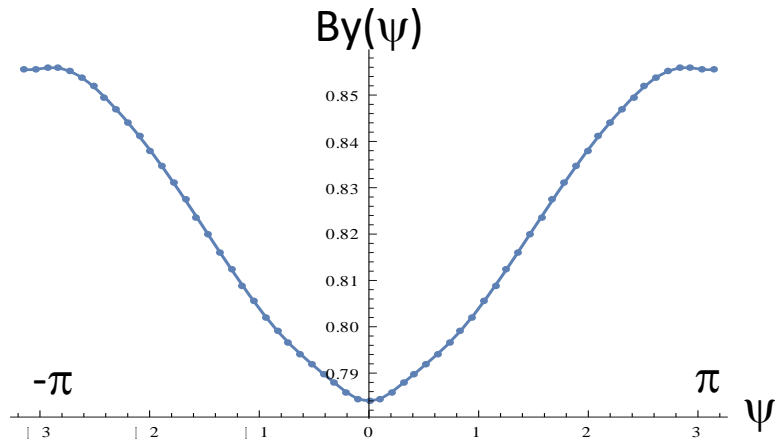
Elliptical multipoles

$$\mathbf{B}(\mathbf{z})/\mathcal{B}_0 = \sum_{m=0}^{\infty} \mathbf{C}_m \left(\frac{x+iy}{R}\right)^m = \sum_{m=0}^{\infty} \mathbf{C}_m \alpha^m \cosh^m \mathbf{w} \quad (29)$$

$$\begin{aligned} \alpha^m \mathbf{C}_m &= \sum_{k=0}^{\infty} \mathbf{E}_k / [(1 + \delta_{k0}) \cosh(k\eta_0)] t_{km}, \\ k, m &= 0, 1, 2, \dots \end{aligned} \quad (34)$$

$$\begin{aligned} m = \text{even: } t_{km} &= (-1)^{m/2} \cos(k\pi/2) \frac{1}{m!} \\ &\quad \times \prod_{\mu=1}^{m/2} (k^2 - [2(\mu-1)]^2) \end{aligned} \quad (36)$$

$$\begin{aligned} m = \text{odd: } t_{km} &= (-1)^{(m-1)/2} \sin(k\pi/2) \frac{k}{m!} \\ &\quad \times \prod_{\mu=1}^{(m-1)/2} (k^2 - (2\mu-1)^2). \end{aligned} \quad (37)$$



Ra=20mm **semi-major axis**
Rb=8mm **semi-minor axis**
r=15mm **radius of circular multipoles expansion**

$$m = \text{even: } t_{km} = (-1)^{m/2} \cos(k\pi/2) \frac{1}{m!} \times \prod_{\mu=1}^{m/2} (k^2 - [2(\mu - 1)]^2) \quad (36)$$

$$m = \text{odd: } t_{km} = (-1)^{(m-1)/2} \sin(k\pi/2) \frac{k}{m!} \times \prod_{\mu=1}^{(m-1)/2} (k^2 - (2\mu - 1)^2). \quad (37)$$

Transfer matrix of even multipoles from elliptical multipoles to circular multipoles

Out[25]/MatrixForm=

m=even: t_{km} =

$\frac{1}{2}$	-0.724138	0.355359	-0.156465	0.0673952	-0.0289105	0.0123923	-0.00531116	0.00227622	-0.000975526
0	0.969828	-1.90371	1.88596	-1.44418	0.967985	-0.597487	0.348545	-0.195105	0.105827
0	0	1.2748	-3.36779	4.83543	-5.18563	4.66787	-3.73441	2.74366	-1.88977
0	0	0	1.50348	-5.18082	9.72306	-13.3368	15.0043	-14.6982	12.9922
0	0	0	0	1.73465	-7.44112	17.2238	-28.7073	38.6671	-44.7434
0	0	0	0	0	1.99316	-10.2523	28.1946	-55.2388	86.5573
0	0	0	0	0	0	2.28845	-13.7311	43.7157	-98.3605
0	0	0	0	0	0	0	2.62713	-18.0147	65.1426
0	0	0	0	0	0	0	0	3.01586	-23.2652
0	0	0	0	0	0	0	0	0	3.46209

Transfer matrix of odd multipoles from elliptical multipoles to circular multipoles

Out[31]/MatrixForm=

m=odd: t_{km} =

0.75	-1.27703	0.969941	-0.588815	0.325152	-0.170386	0.0863055	-0.0426791	0.0207299	-0.00992946
0	1.1402	-2.59806	3.15437	-2.90315	2.28195	-1.61823	1.06698	-0.666319	0.398952
0	0	1.39182	-4.2246	6.99865	-8.55732	8.66908	-7.71654	6.24674	-4.70193
0	0	0	1.61656	-6.2488	13.0979	-19.9035	24.6063	-26.2937	25.1889
0	0	0	0	1.85976	-8.77094	22.2137	-40.2782	58.6912	-73.0928
0	0	0	0	0	2.13578	-11.9002	35.3088	-74.3168	124.59
0	0	0	0	0	0	2.45197	-15.7629	53.5939	-128.355
0	0	0	0	0	0	0	2.8148	-20.5079	78.5848
0	0	0	0	0	0	0	0	3.23128	-26.3119
0	0	0	0	0	0	0	0	0	3.70938

Out[40]//MatrixForm=

Number of circular multipole	Value
0	0.823442
1	-1.78526
2	-3.34124
3	10.8776
4	815.01
5	-24 229.7
6	-8.42796×10^6
7	2.9995×10^8
8	1.35615×10^{10}
9	-3.02063×10^{12}
10	-4.08203×10^{14}
11	1.38306×10^{16}
12	3.82107×10^{18}
13	1.84429×10^{19}
14	-4.85593×10^{22}
15	-1.19821×10^{24}
16	4.60038×10^{26}
17	1.357×10^{28}
18	-3.19484×10^{30}
19	-9.45785×10^{31}
20	1.6015×10^{34}
21	4.57078×10^{35}
22	-5.70995×10^{37}
23	-1.55765×10^{39}
24	1.40731×10^{41}
25	3.67578×10^{42}
26	-2.26729×10^{44}
27	-5.72312×10^{45}
28	2.132×10^{47}
29	5.29547×10^{48}
30	-8.78788×10^{49}
31	-2.20595×10^{51}

$$\alpha^m \mathbf{C}_m = \sum_{k=0}^{\infty} \mathbf{E}_k / [(1 + \delta_{k0}) \cosh(k\eta_0)] t_{km},$$

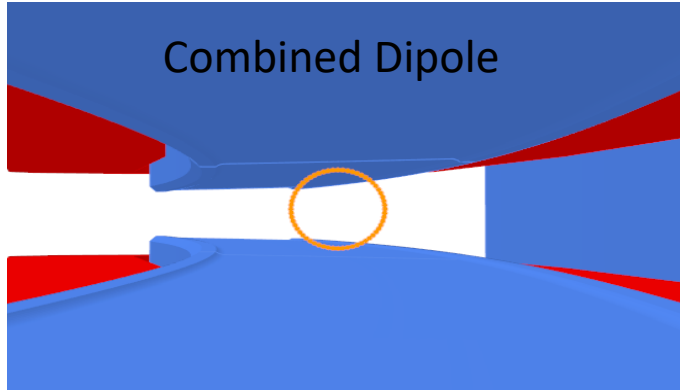
$$k, m = 0, 1, 2, \dots$$

(34)

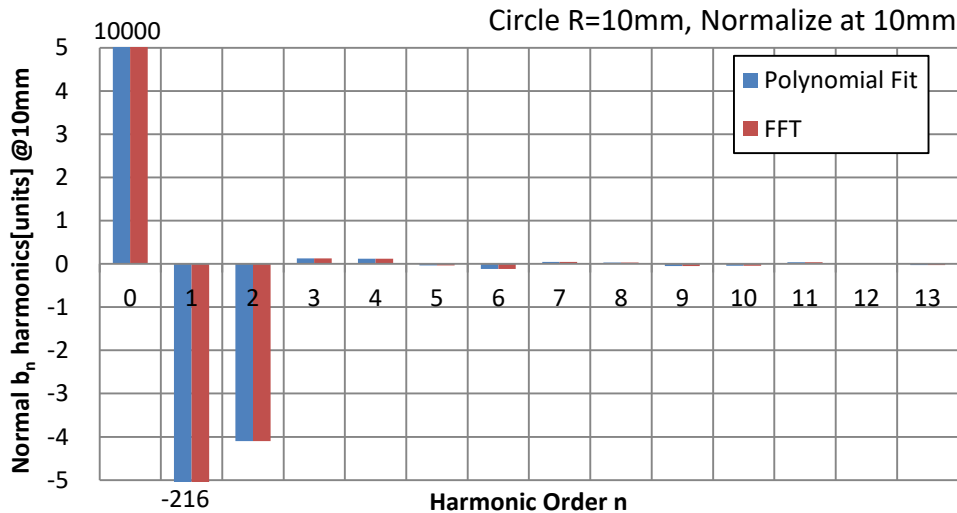
Simulation Case

Circular path data of a combined dipole

Simulation of Multipoles in a circle



Combined Dipole	Main components	Normalize to $b_0(x10^{-4}) @10mm$
b_0	0.823 T	10000
b_1	-1.79 T/m	-216.8
b_2	-3.38 T/m ²	-4.1



- The multipole results of polynomial fit and FFT are the same in a circular path at a combined dipole.
- Shows two analysis methods are consistence in a circular path.

12

Circle	Polynomial	FFT
b_0	0.8234427 T	0.823443 T
b_1	-1.785341 T/m	-1.785342 T/m
b_2	-3.376005 T/m ²	-3.375895 T/m ²

Combined Dipole Magnet

Circular Path

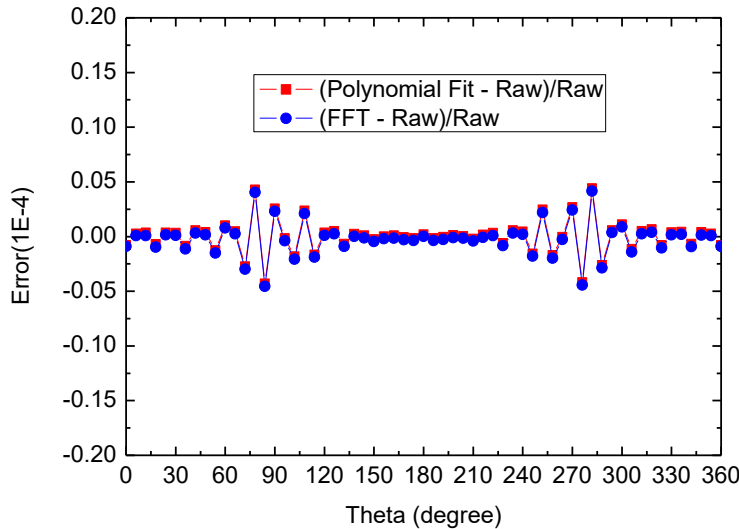
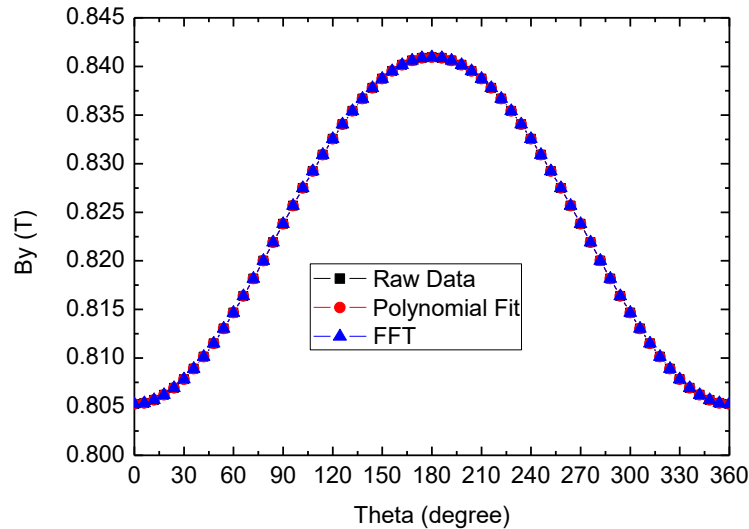
R=10mm

$b_n \setminus a_n$ into

$$B_y(\theta) = \sum r^n [b_n \cos(n\theta) - a_n \sin(n\theta)]$$

or

$$B_y(x,y) = b_0 + a_1 y + b_1 x + 2a_2 xy + b_2(x^2 - y^2) + \dots$$

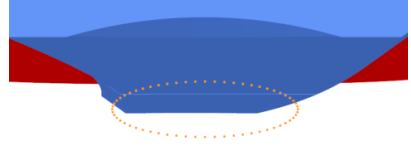


- The errors of these two methods are within 5×10^{-6} .

Simulation Case

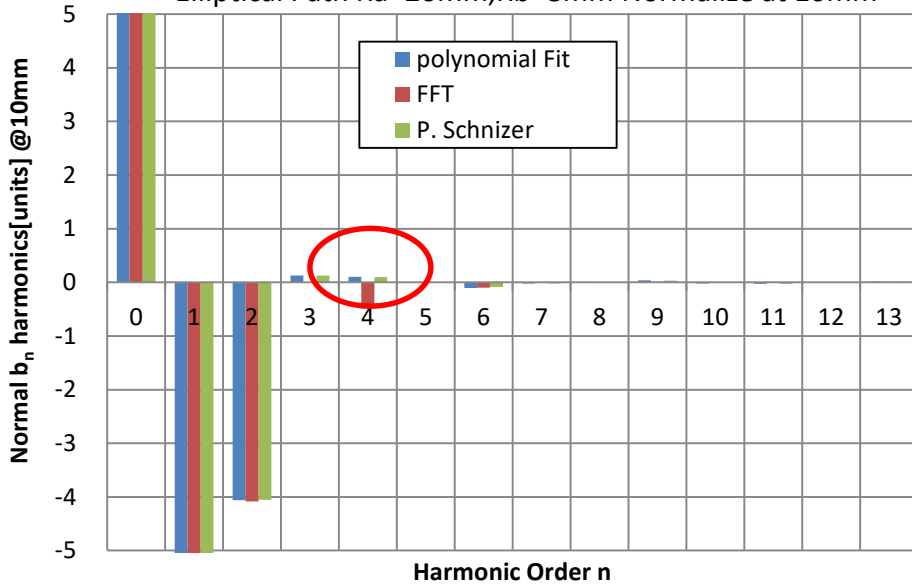
Elliptical path data of a combined dipole

Elliptical Path Analysis

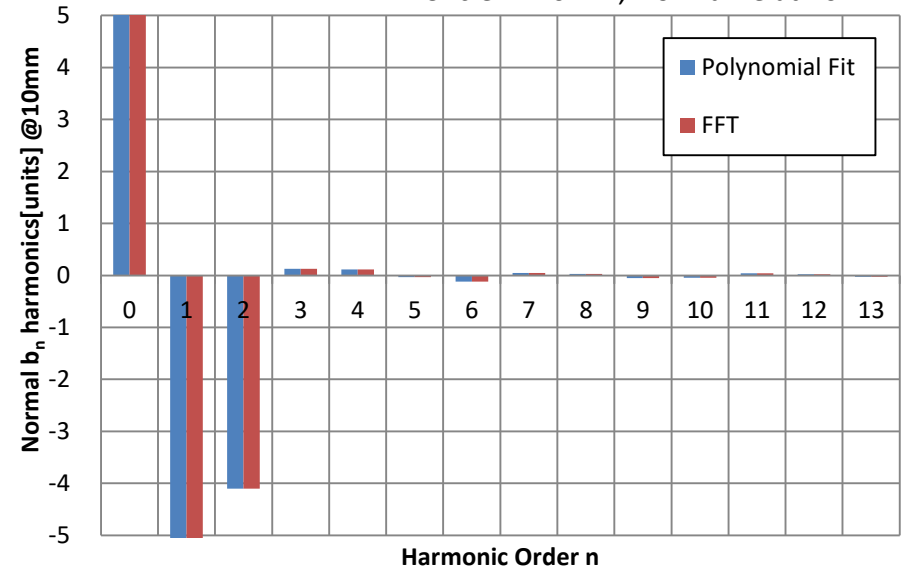


Combined Dipole

Elliptical Path $R_a=20\text{mm}, R_b=8\text{mm}$ Normalize at 10mm



Circle $R=10\text{mm}$, Normalize at 10mm

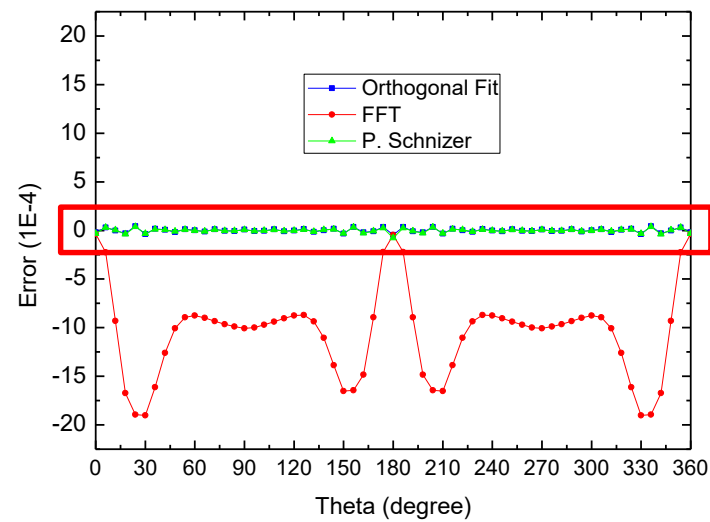
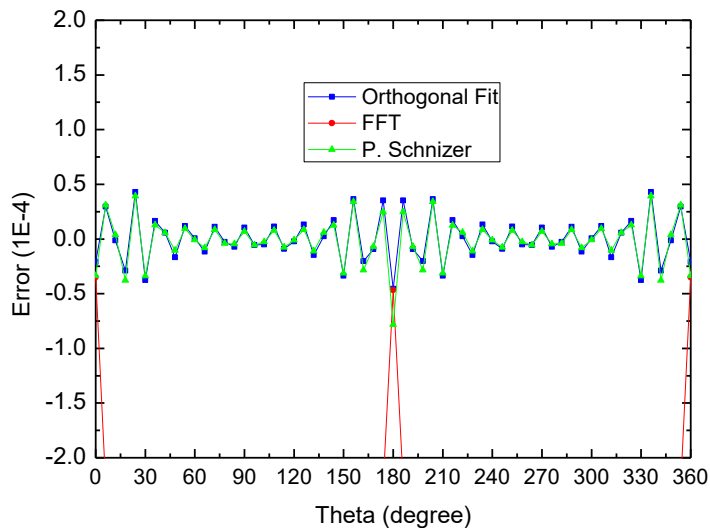
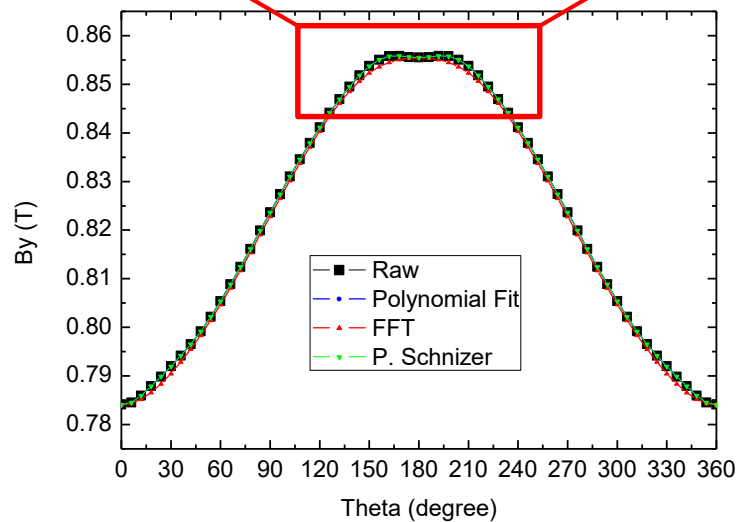
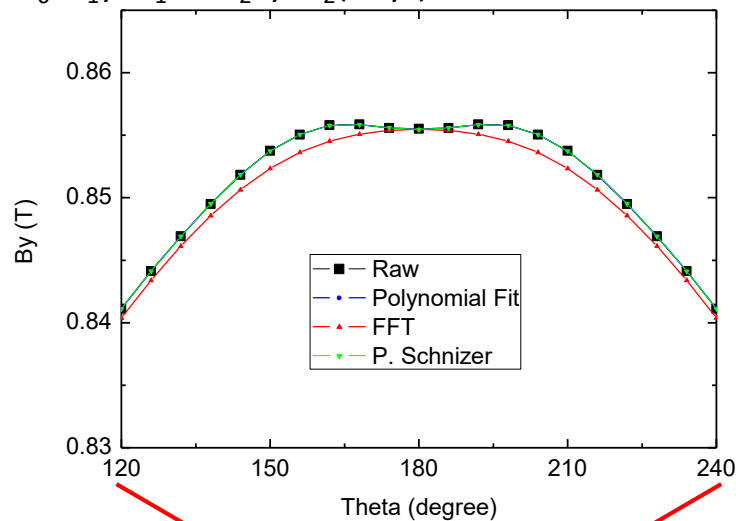


Ellipse	Polynomial	FFT	P. Schnizer
b_0	0.8234423 T	0.822633 T	0.823442 T
b_1	-1.785267 T/m	-1.784512 T/m	-1.78526 T/m
b_2	-3.341436 T/m ²	-3.359222 T/m ²	-3.34125 T/m ²

Circle	Polynomial	FFT
b_0	0.8234427 T	0.823443 T
b_1	-1.785341 T/m	-1.785342 T/m
b_2	-3.376005 T/m ²	-3.375895 T/m ²

Elliptical path $b_n \setminus a_n$ into

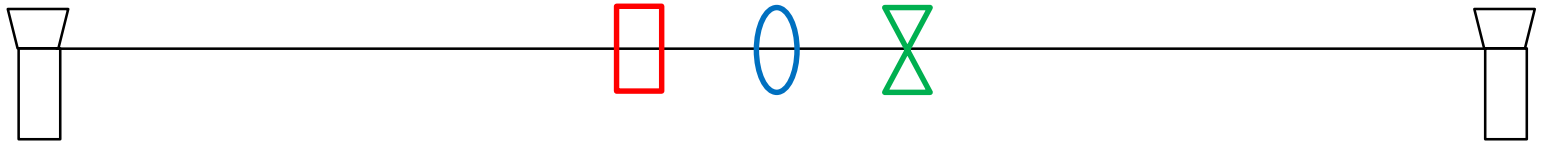
$$By(x,y)=b_0+a_1y+b_1x+2a_2xy+b_2(x^2-y^2)+...$$



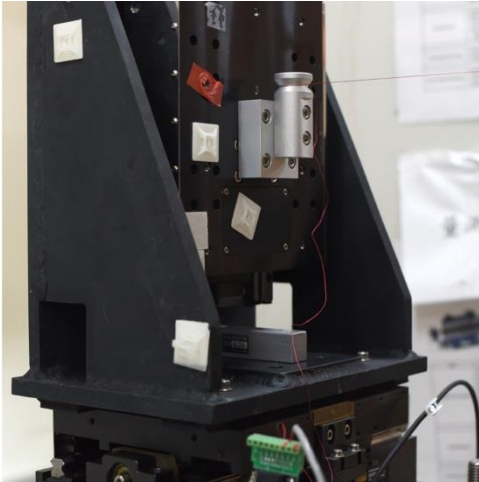
Analysis Conclusion

- The multipole results of polynomial fit and FFT are the same in a circular path at a combined dipole. The errors of these two methods are within 5×10^{-6} .
- Polynomial fit, FFT and P. Schnizer in an ellipse are compared, polynomial fit result is the same as P. Schnizer, FFT multipole got a large errors. So we can chose polynomial fit or P. Schnizer anaylsis method for multipoles in an ellipse.
- The fitting errors of polynomial fit and P. Schnizer of elliptical path are within 5×10^{-5} .

Stretched wire system



Stretched Wire System Setup



Parameter	Value	Units
Wire length	1100	mm
Wire diameter	0.3	mm
Wire mass density	0.4	g/m
Wire sag	0.25	mm

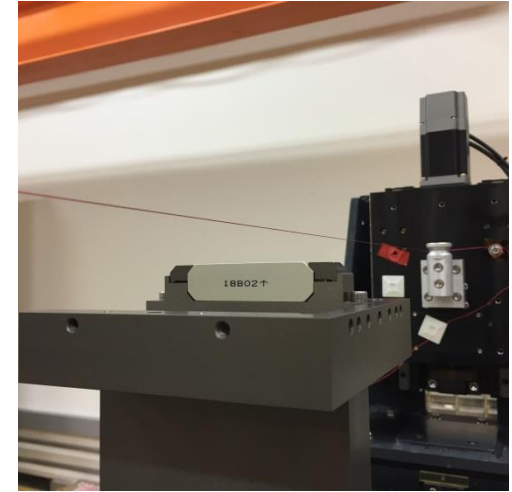
Parameters of 8 turns copper wires.

- Integrator and voltmeter (Keithley2182) testing results are very close.
- The movement of transverse and vertical direction are moving by stepping motors.
- The wires are stretched by moving the stage longitudinal manually.
- Mechanical centre can be found by level meter and theodolite.
- 8 turns copper wires are in series.

Standard deviation at one position

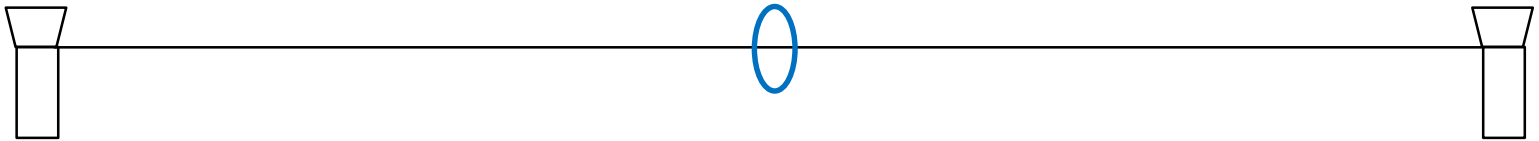
STDEV	Voltmeter KEITHLEY 2182	Integrator FDI 2056
Be-Cu wire dx=2mm	3.0 G-cm	2.9 G-cm
Be-Cu wire dx=4mm	2.0 G-cm	-
8 Cu wires dx=2mm	1.0 G-cm	1.0 G-cm
8 Cu wires dx=4mm	0.5 G-cm	0.5 G-cm

Move step dx (mm)	STDEV (G-cm)	8Cu wires With FDI2056 v=25 mm/s } Poor space resolution
1	2	
2	1	
4	0.5	
6	0.2	
8	0.3	



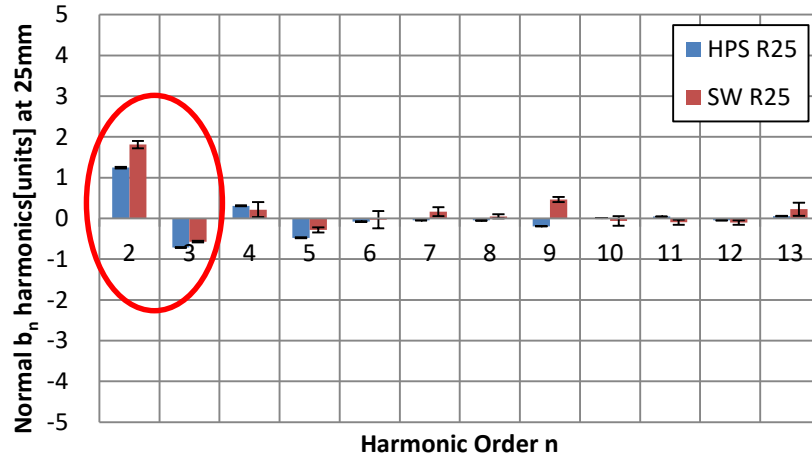
Ref. NdFeB Block
By(x=0mm)=3300 G-cm

Integral multipoles of a quadrupole magnet by stretched wire system

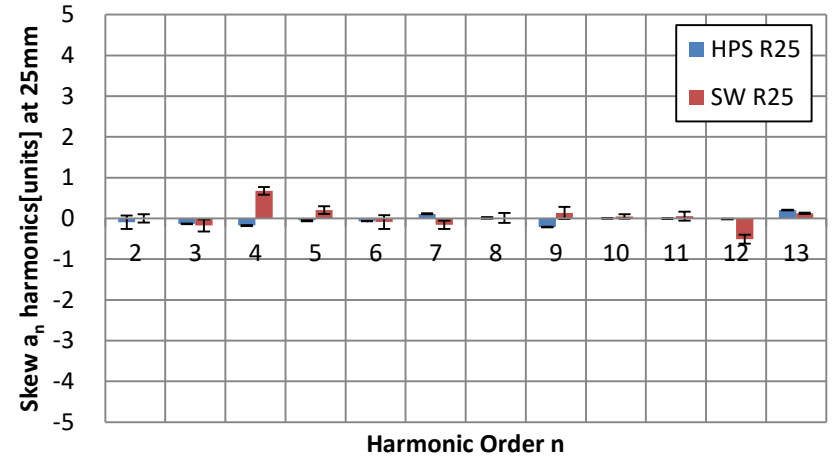


QM R25mm HPS & SW Experimental Results

Normal bn harmonics



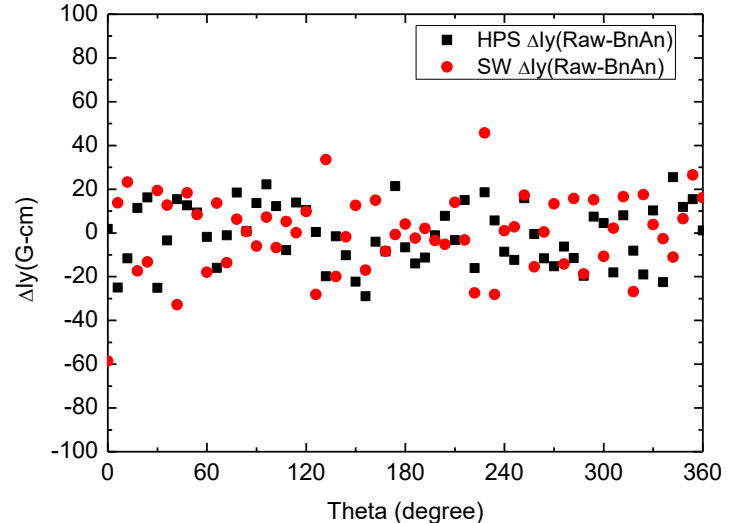
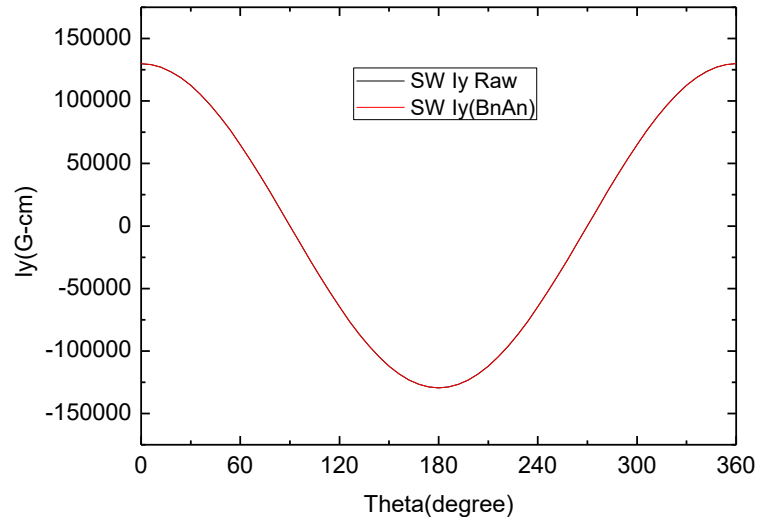
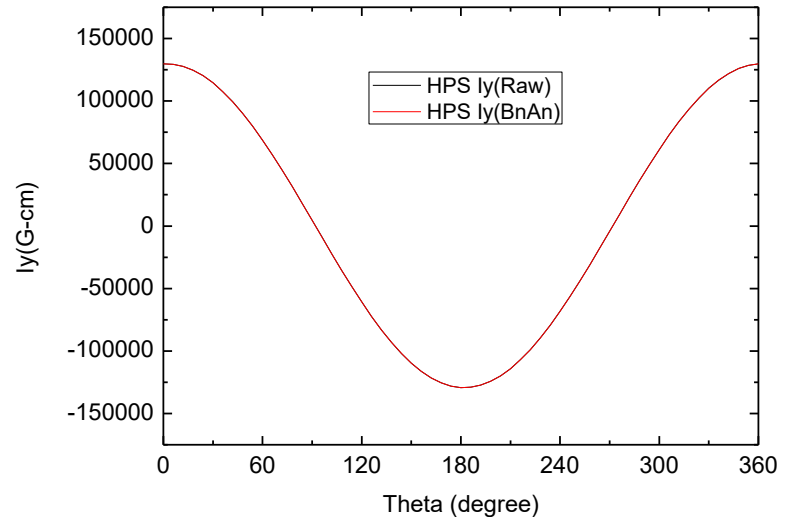
Skew an harmonics



Circle R=25mm, Normalize at 25mm

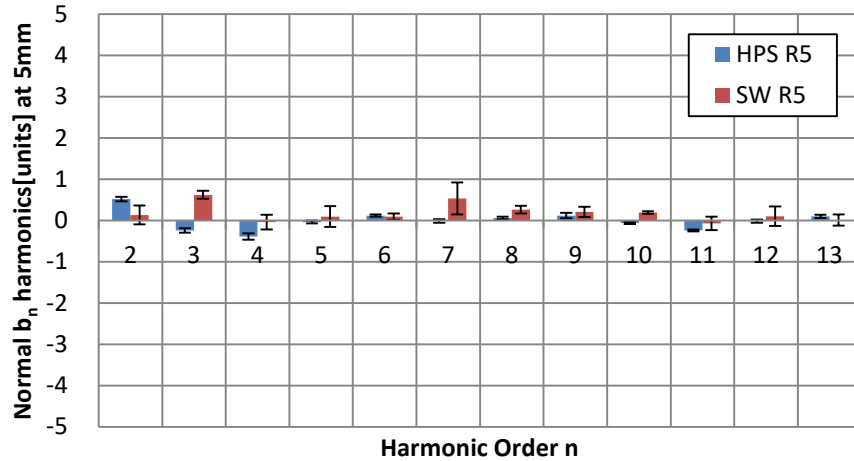
System	$\int Gdz$ (T)
HPS	5.178
SW	5.179

- Normal sextupole(b2) and octupole (b3) are particular multipole.
- The difference of all multipole are within 1 units between HPS and SW.

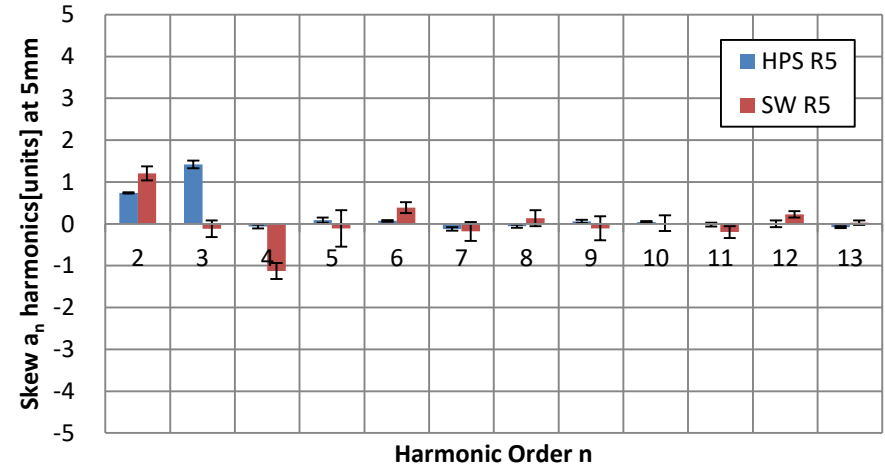


R5mm HPS vs SW

Normal b_n harmonics



Skew a_n harmonics



Circle R=5mm, Normalize at 5mm

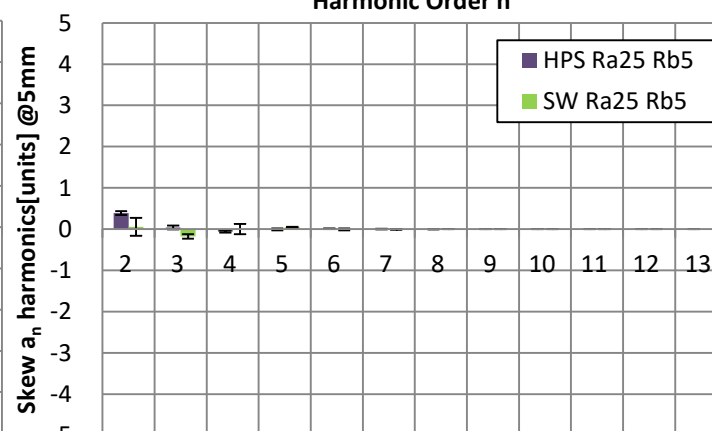
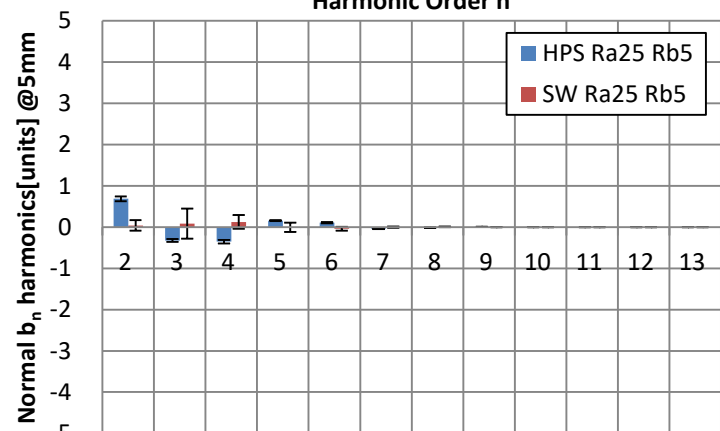
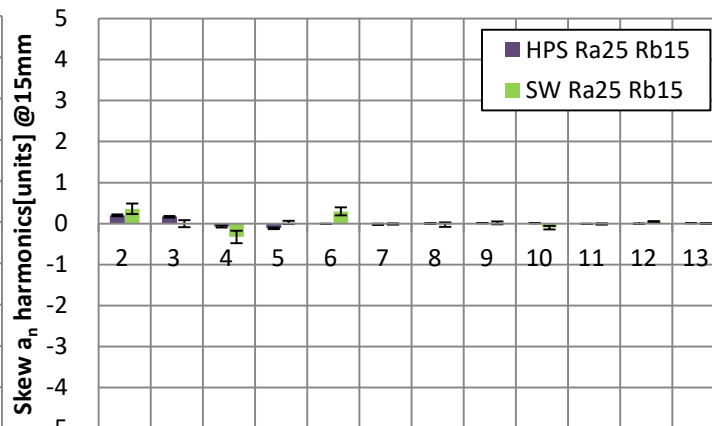
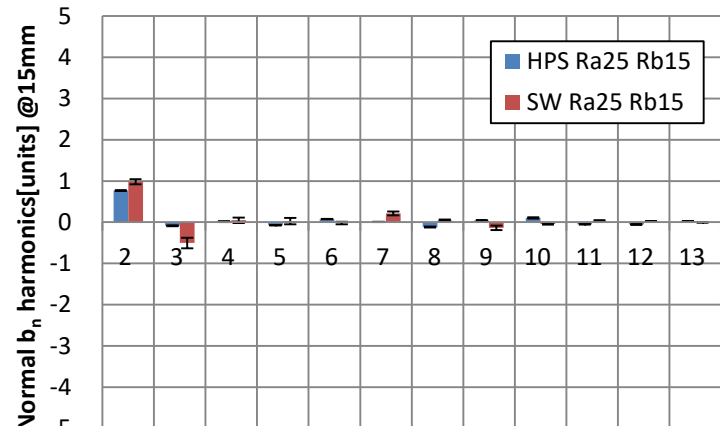
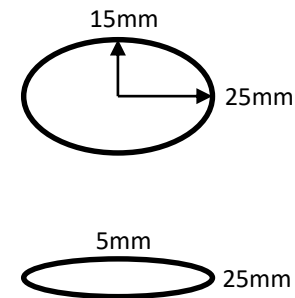
System	$\int Gdz$ (T)
HPS	5.177
SW	5.178

- The deviation of R5 data is larger than R25.
- The difference is within 2 units between HPS and SW.

Elliptical Path HPS vs SW

Normal b_n harmonics

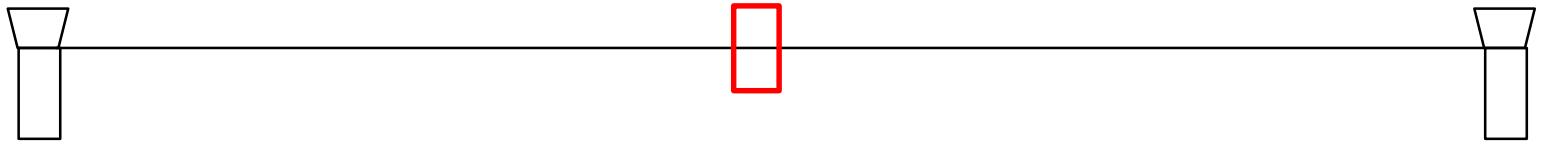
Skew a_n harmonics



HPS/SW Path	$\int Gdz$ (T)
HPS Ellipse Ra25 Rb15	5.177
HPS Ellipse Ra25 Rb5	5.176
SW Ellipse Ra25 Rb15	5.174
SW Ellipse Ra25 Rb5	5.176

Normalize at short axis radius

Integral multipoles of in-vacuum undulator by stretched wire system

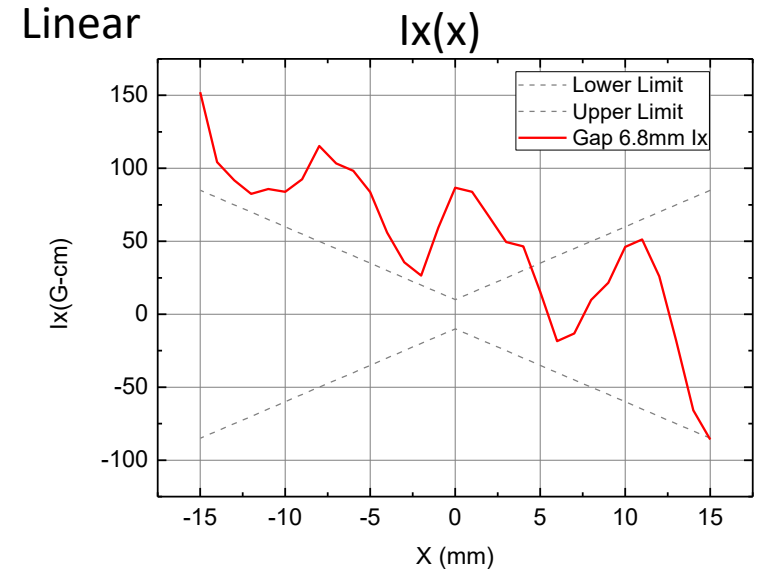
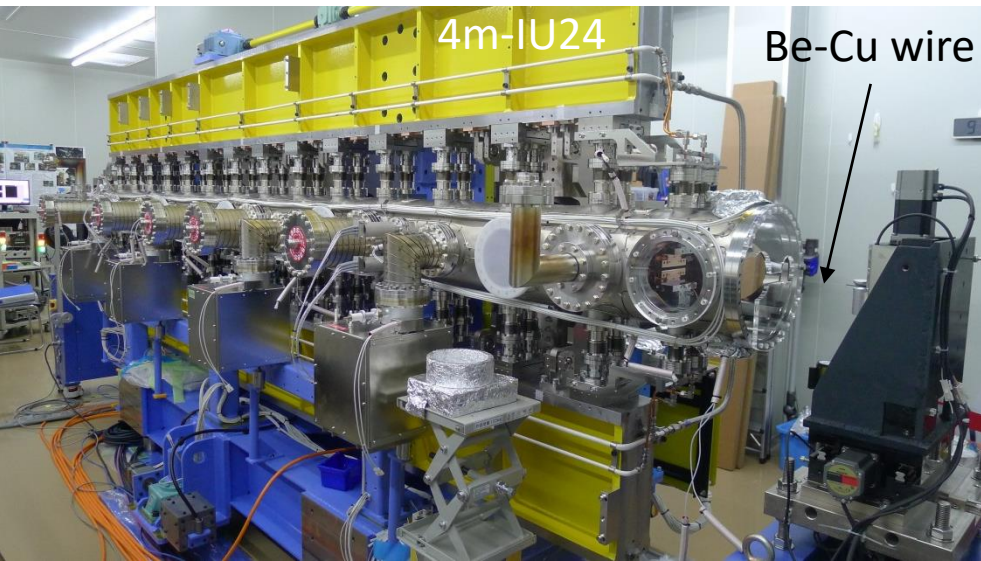


IU24 Linear & Elliptical measurement

To check skew quadrupole value which is out of spec.

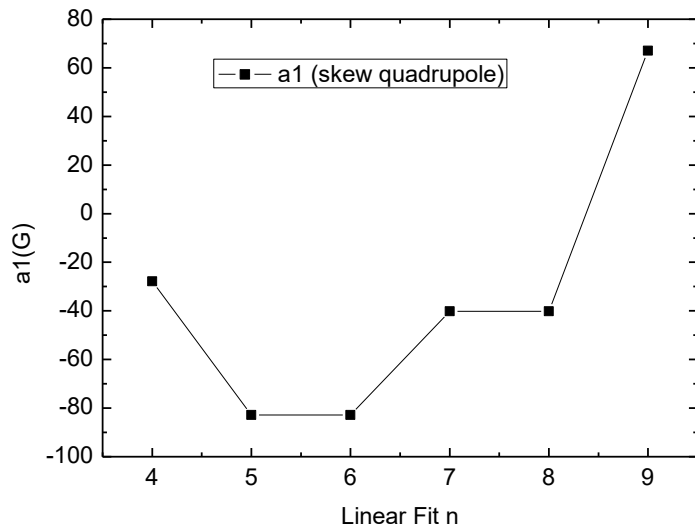
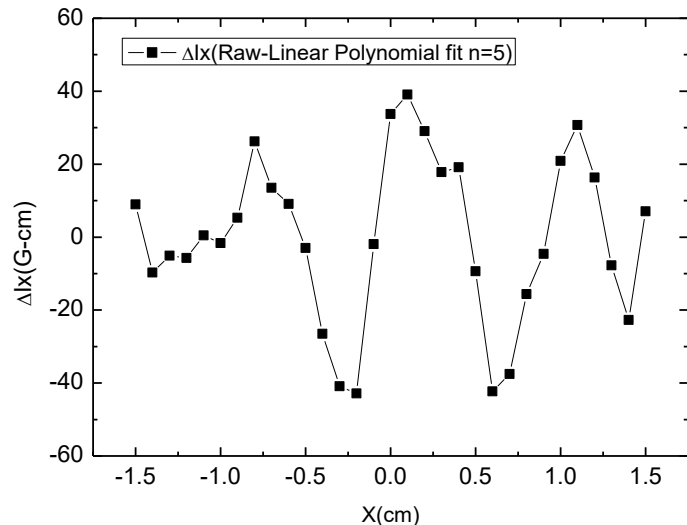
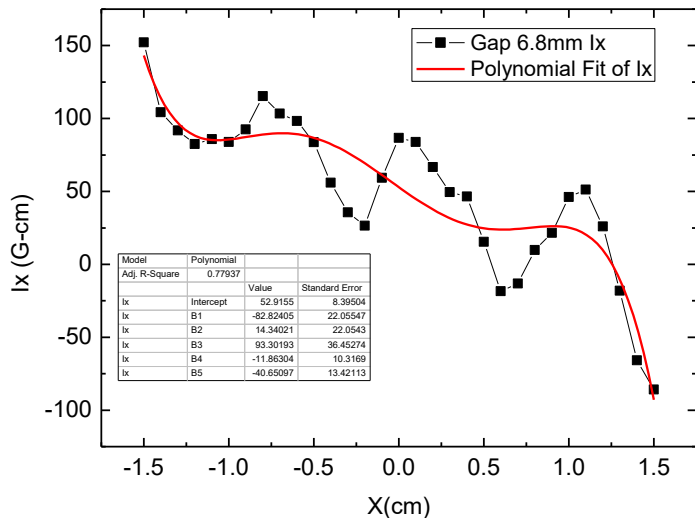
-15 < x < 15 (mm)		Linear Measurement		
Gap(mm)		Dipole(n=0)	Quadrupole(n=1)	Sextupole(n=2)
Spec.		≤100 G-cm	≤50 G	≤100 G/cm
6.8	Normal(Iy)	-3.9	34.1	14.1
	Skew(Ix)	62.2	-79.8	-8.1
7	Normal(Iy)	-11.7	38.5	15.4
	Skew(Ix)	50.5	-82.3	16.7
8	Normal(Iy)	-28.9	26.3	14.6
	Skew(Ix)	48.8	-60.2	18.5
9	Normal(Iy)	-38.8	29.6	16.2
	Skew(Ix)	52.4	-41.2	3.6

Elliptical Measurement				
Gap(mm)		Dipole(n=0)	Quadrupole(n=1)	Sextupole(n=2)
Spec.		≤100 G-cm	≤50 G	≤100 G/cm
6.8	Normal	0.4	47.1	43.1
	Skew	-	-105.7	29.8
7	Normal	-6.0	36.0	33.2
	Skew	-	-78.7	21.3
8	Normal	-21.8	48.5	68.0
	Skew	-	-73.4	16.1
9	Normal	-34.3	49.6	61.4
	Skew	-	-44.8	35.8



IU24 Gap 6.8mm

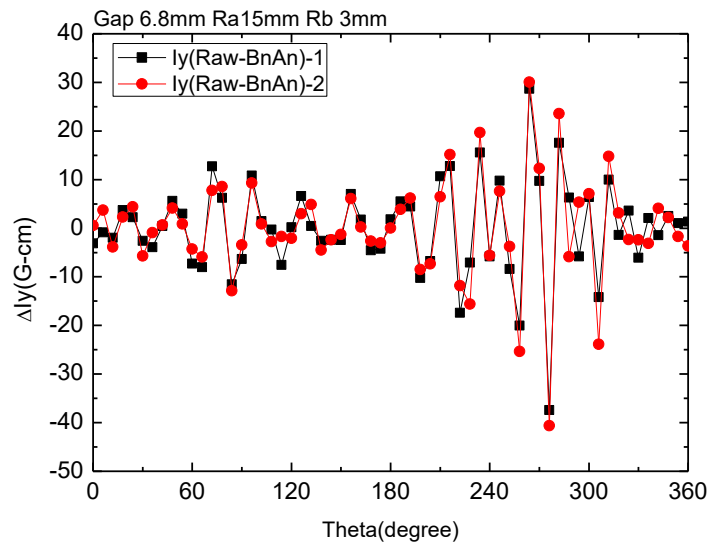
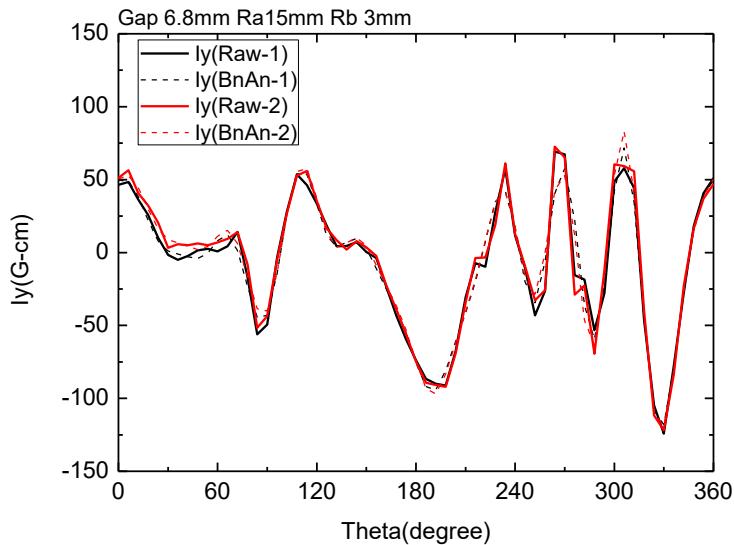
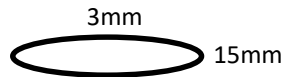
Linear



- It is hard to confirm skew quadrupole value.
- Different linear polynomial fit number get different results.

IU24 Gap 6.8mm

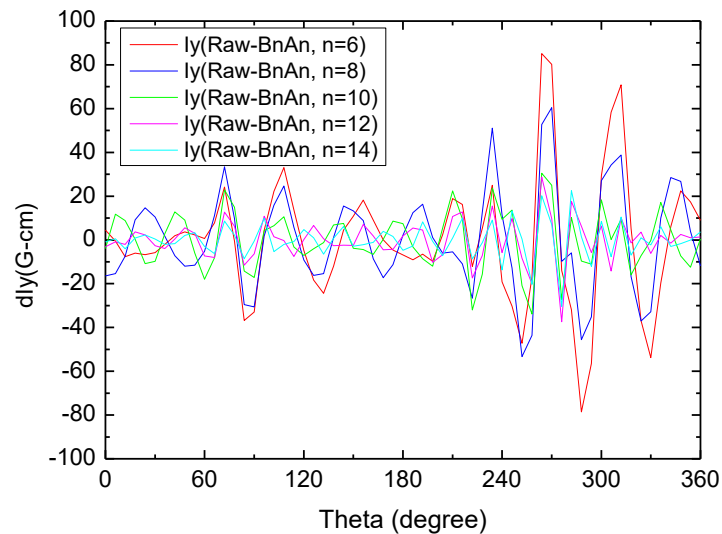
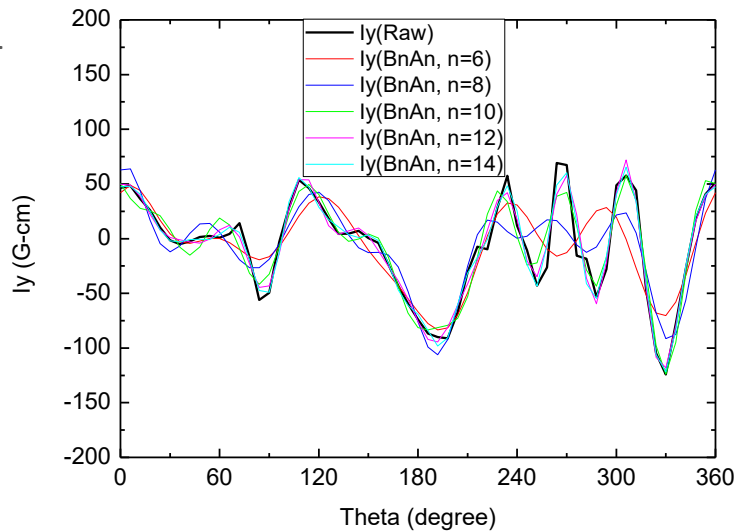
Elliptical path polynomial fit



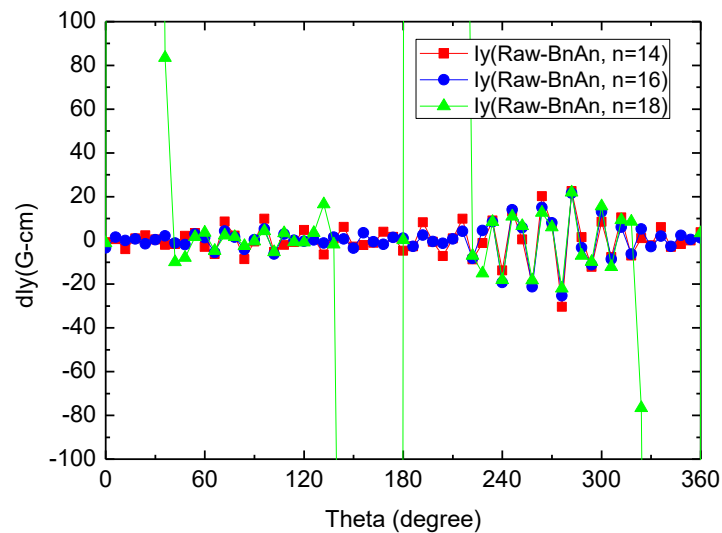
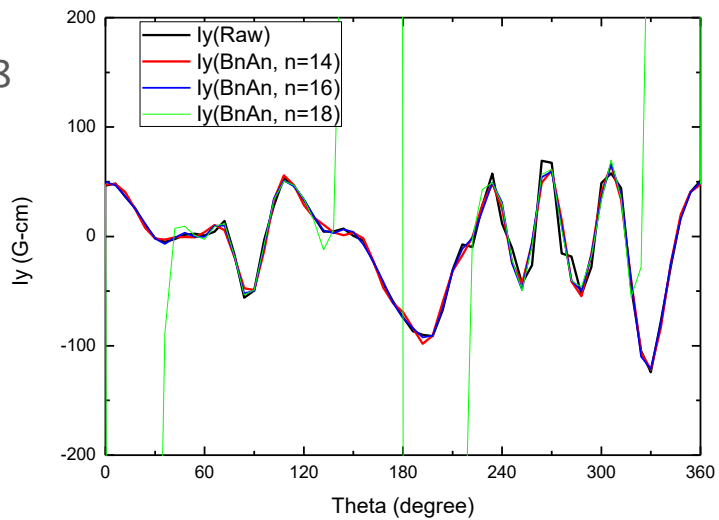
Raw data $ly(x,y)$ still was looked like unusually but elliptical path polynomial fit well.

Elliptical path Fitting number

N=6~14

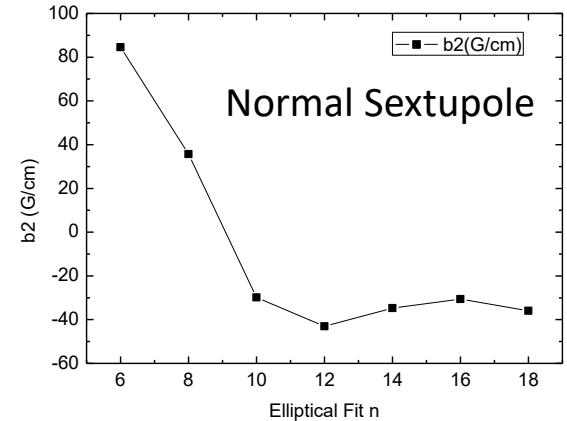
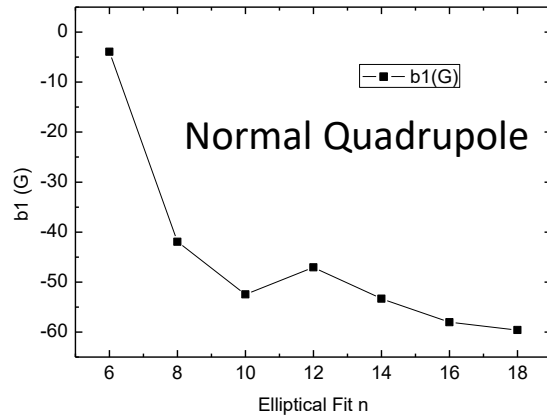
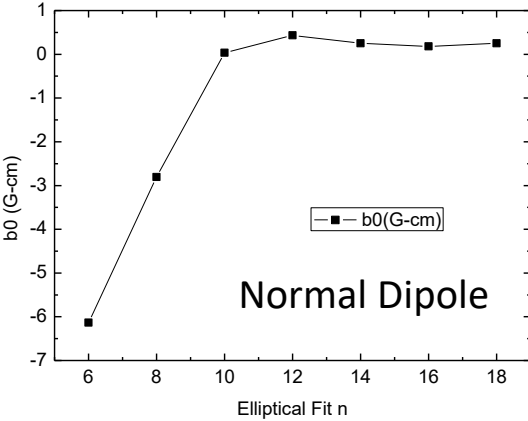


N=14~18



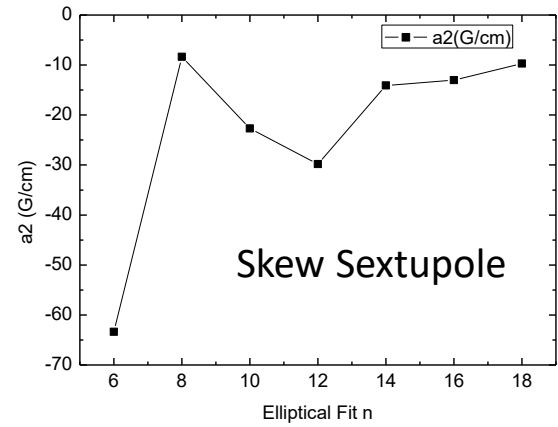
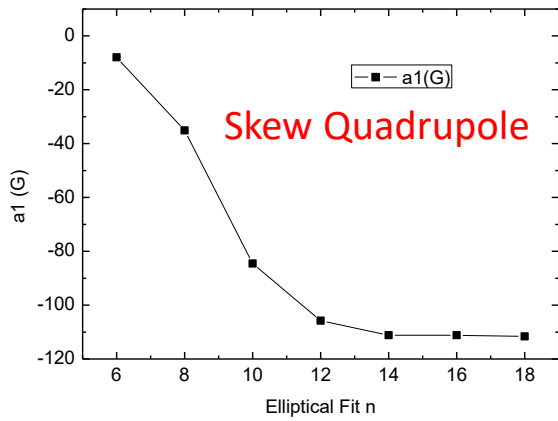
Elliptical path Fitting number

Normal Terms

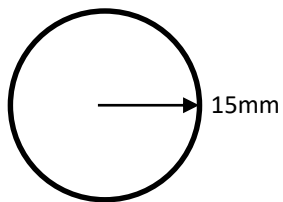


Skew Terms

b0, b1, b2, a1, a2 are convergent.



IU24 Gap 40mm Circle & Ellipse

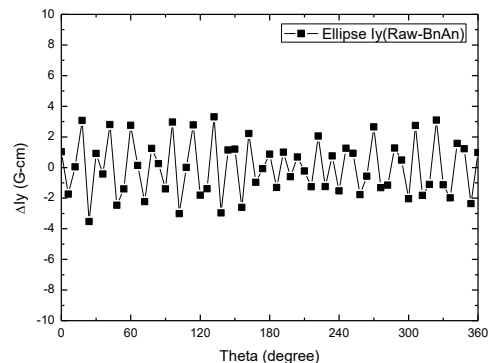
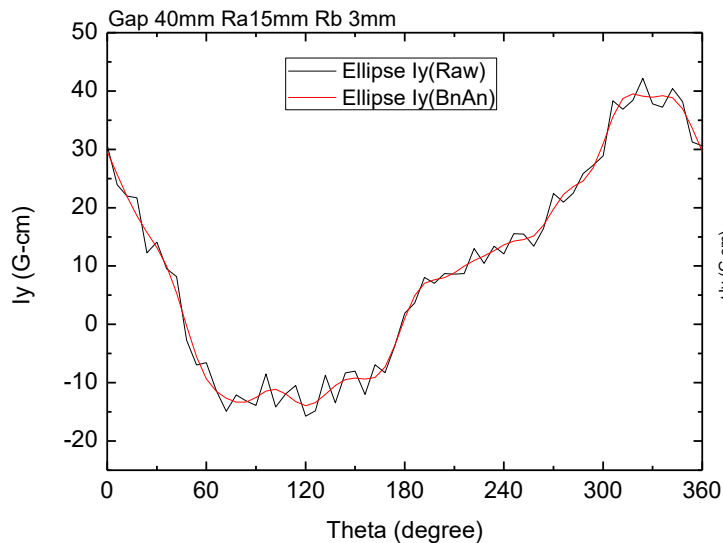
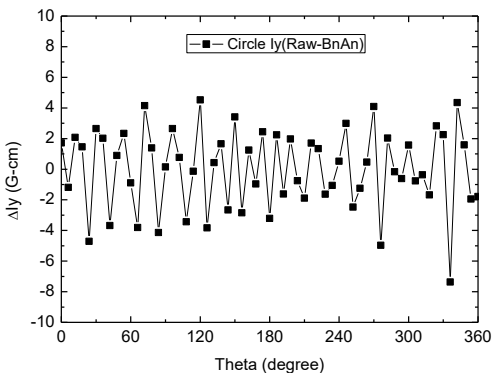
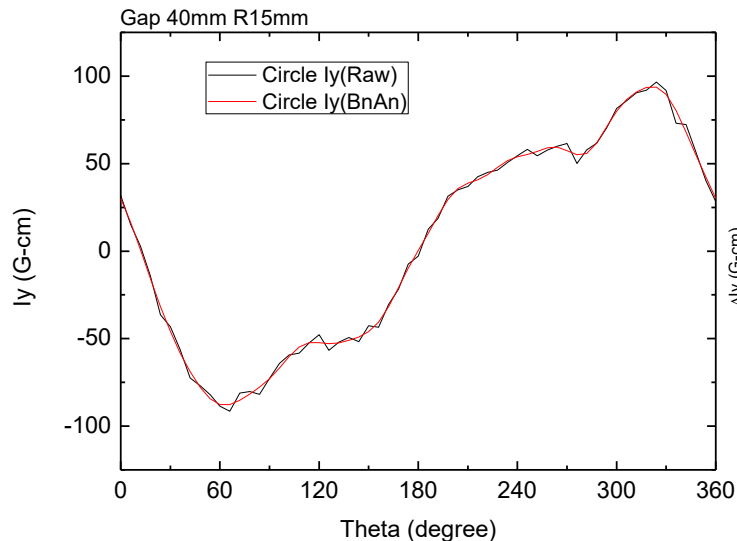
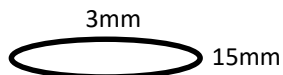


Circle

Gap (mm)		Dipole (n=0)	Quadrupole (n=1)	Sextupole (n=2)
Spec.		≤100 G-cm	≤50 G	≤100 G/cm
40	Normal	3.59	7.40	4.95
	Skew	-	-52.42	-6.94

Ellipse

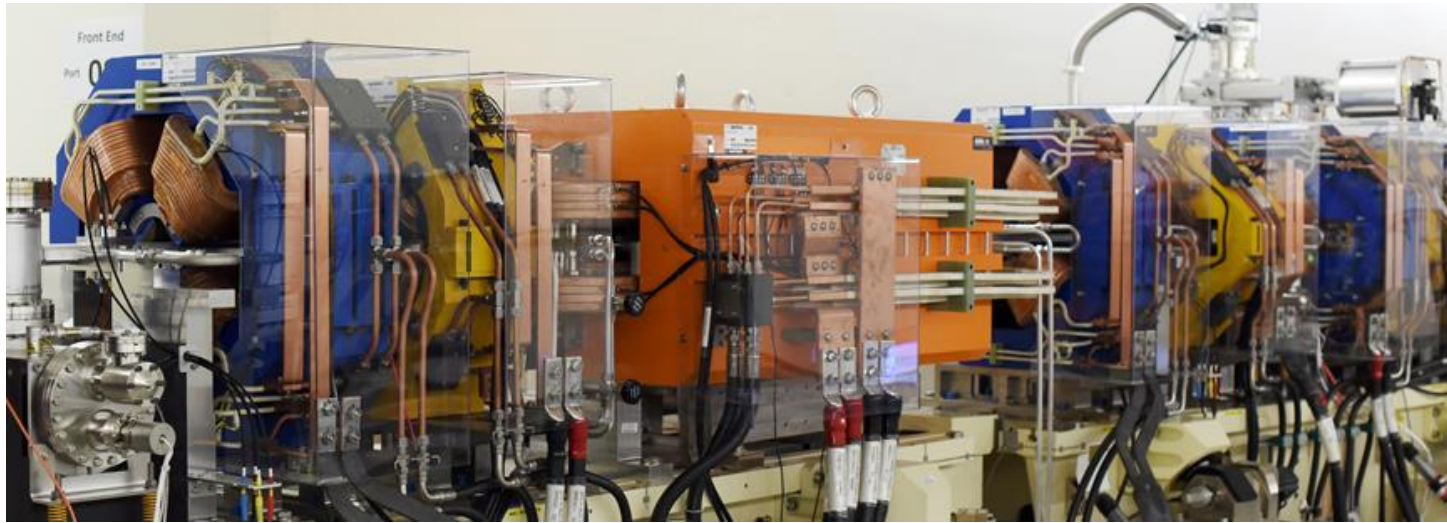
Gap (mm)		Dipole (n=0)	Quadrupole (n=1)	Sextupole (n=2)
Spec.		≤100 G-cm	≤50 G	≤100 G/cm
40	Normal	3.74	5.69	1.59
	Skew	-	-53.85	-16.1



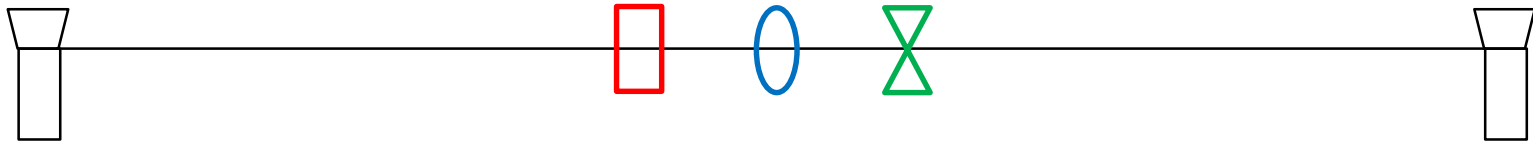
The multipole results are similar in a circle and ellipse.

Conclusions

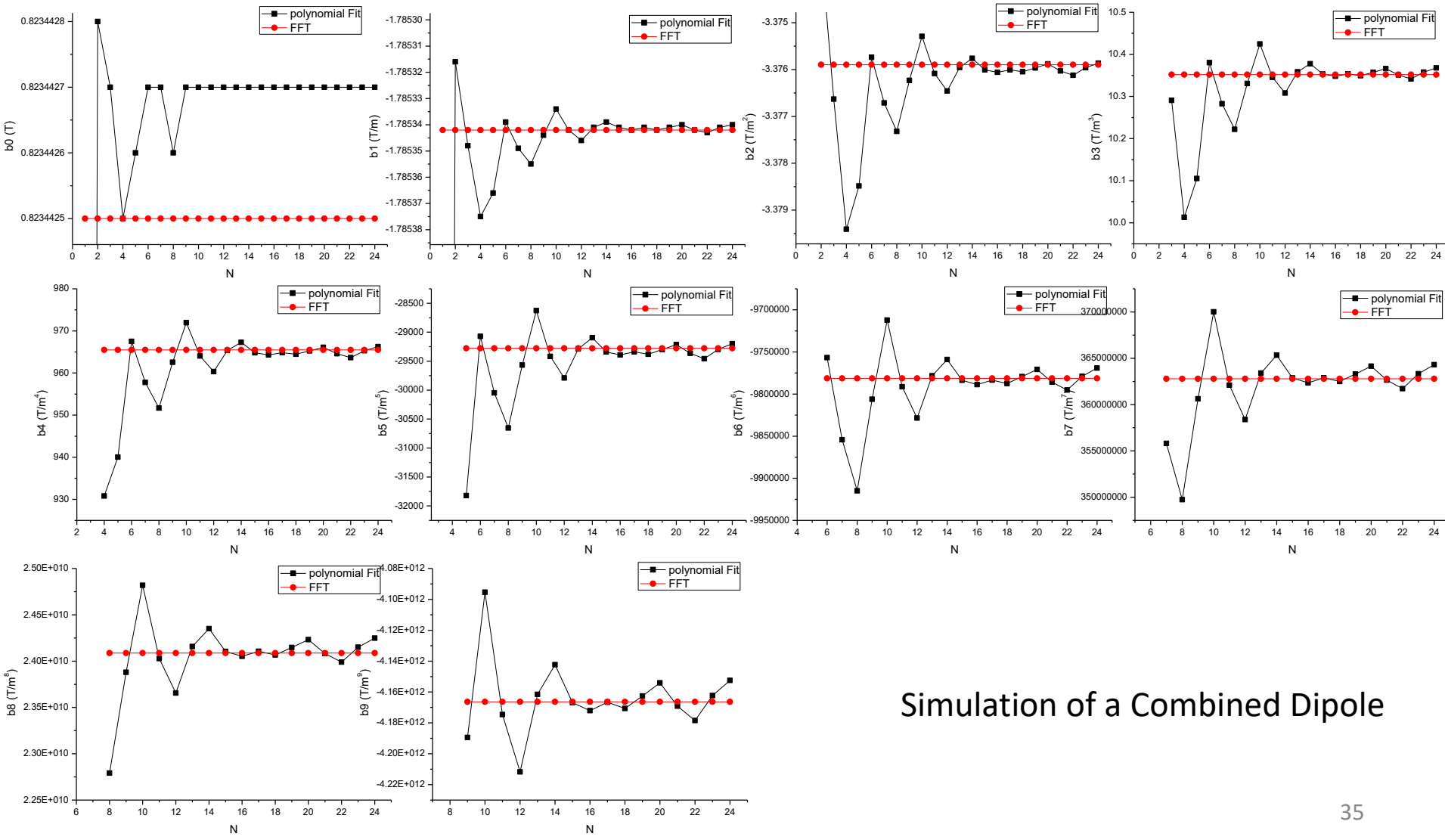
- A quadrupole magnet was measured by Hall probe system and stretched wire system and results were compared. Hall probe system can be more precise but stretched wire system can save lot of time.
- The difference of multipoles are within 2×10^{-4} between Hall probe system and stretched wire system.
- Circular and elliptical measurement of a quadrupole magnet multipoles are showed. If elliptical path multipoles normalized at short radius, the result is similar to circular path multipoles.
- Compare to linear measurement of in-vacuum undulator, elliptical path result shows more easy to confirm the main multipoles($n=0, 1, 2$).
- Stretched wire system not only can measure 1st and 2nd integral fields but also can measure multipoles.



Many Thanks for Your Attention!

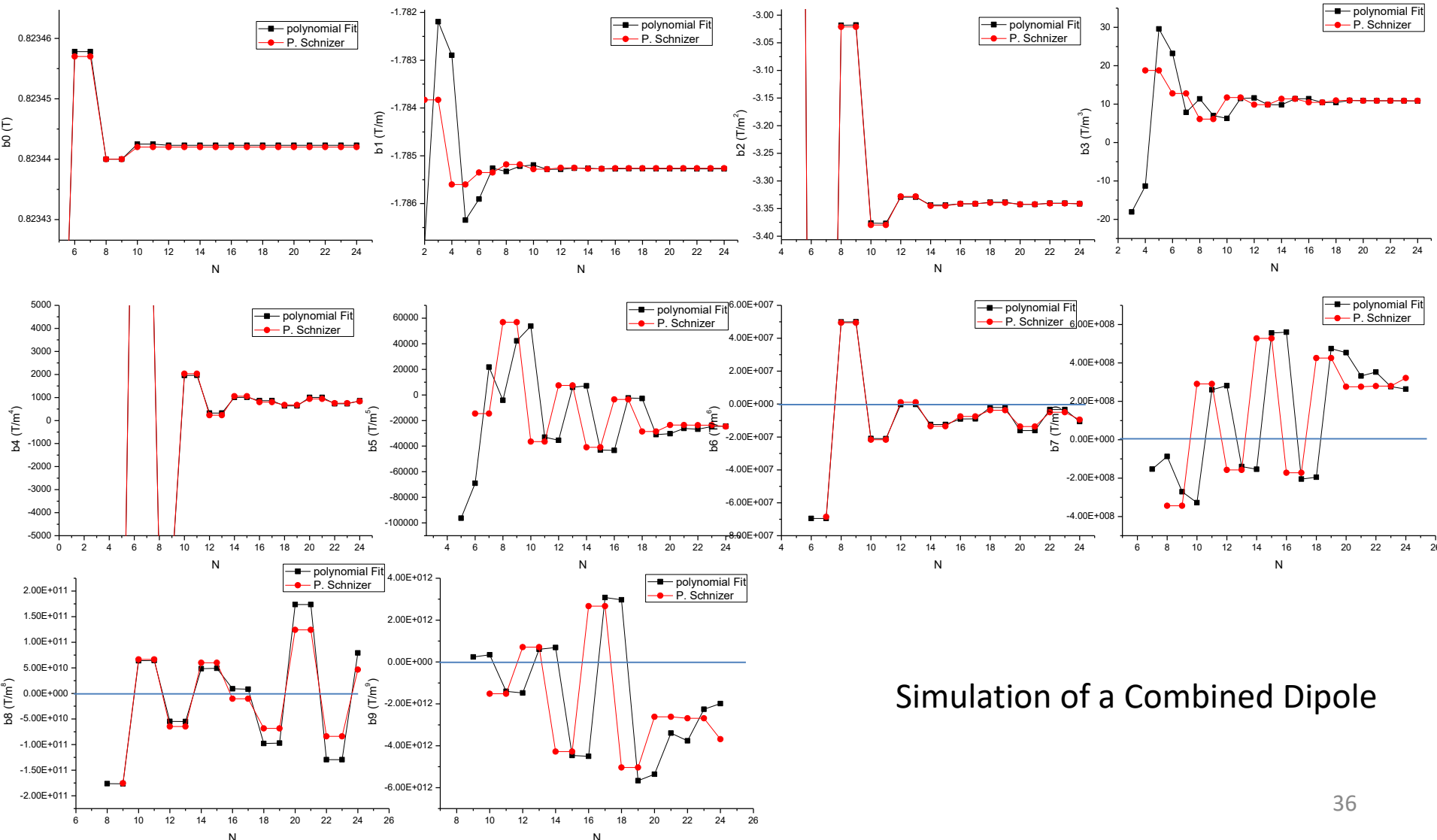


Circle R=10 Fitting Number



Simulation of a Combined Dipole

Ellipse Ra=20 Rb8 Fitting Number



Simulation of a Combined Dipole

Stretched wire measure QM 180A

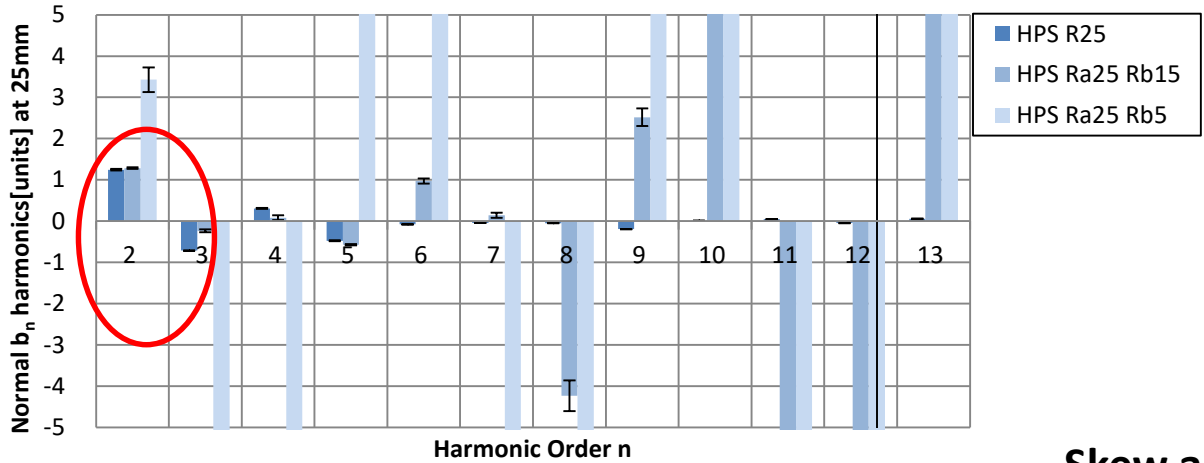
X(mm)	Mean Iy(G-cm)	STDEV (G-cm)	%	
2182	VR=0.1V			
0	124.9331	2.02206	1.618514	v=25mm/s
5	26095.99	2.7032	0.010359	
10	52052.82	3.89971	0.007492	
15	78037.31	7.30075	0.009355	
20	103991.3	4.60909	0.004432	
25	129934.9	10.92665	0.008409	
30	155890.3	8.40531	0.005392	
35	181813.7	10.61701	0.005839	
2182	VR=0.01V			
0	132.9866	2.36717	1.780006	v=15mm/s
5	26003.88	1.66275	0.006394	
10	51875.94	2.98905	0.005762	
15	77733.24	5.94341	0.007646	
20	103612.1	3.71975	0.00359	
25	129462.5	2.62688	0.002029	
30	155297.1	6.77026	0.00436	
35	OVER			
0	124.5182	2.43309	1.954004	v=25mm/s
5	26061.29	1.88915	0.007249	
10	51998.96	1.92215	0.003697	
15	77928.96	3.39732	0.00436	
20	103863.8	5.58763	0.00538	
25	129772.1	9.35304	0.007207	
30	OVER			

FDI2056	G100			
x	Mean Iy(G-cm)	STDEV (G-cm)	%	
0	134.3428	1.80489	1.343496	v=25mm/s
5	26157.84	1.59773	0.006108	
10	52182.57	4.02849	0.00772	
15	78209.52	4.50289	0.005757	
20	104234.9	3.18839	0.003059	
25	130247.2	2.85603	0.002193	
30	156256.7	2.78412	0.001782	
35	182254.6	5.04362	0.002767	

dx=2mm

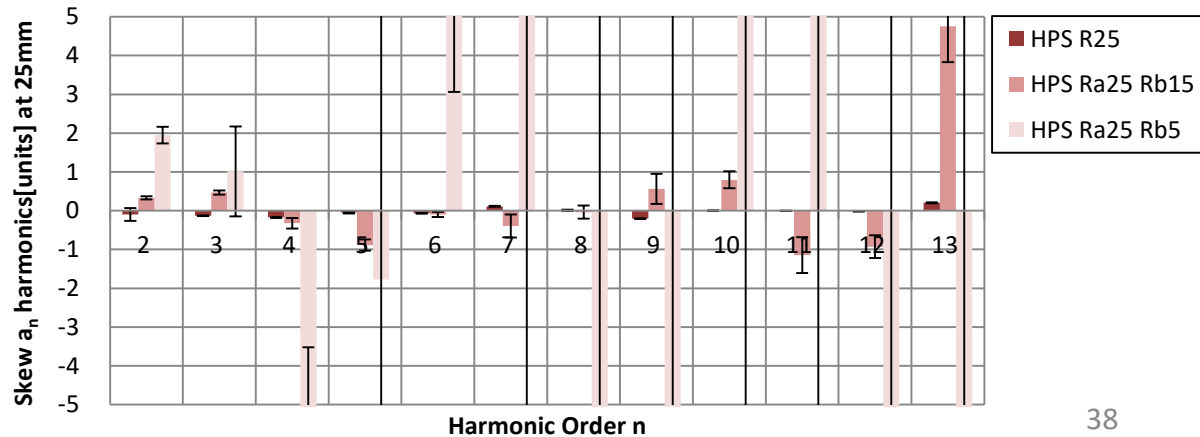
Circle vs Ellipse

Normal b_n harmonics



Normalize at long axis radius

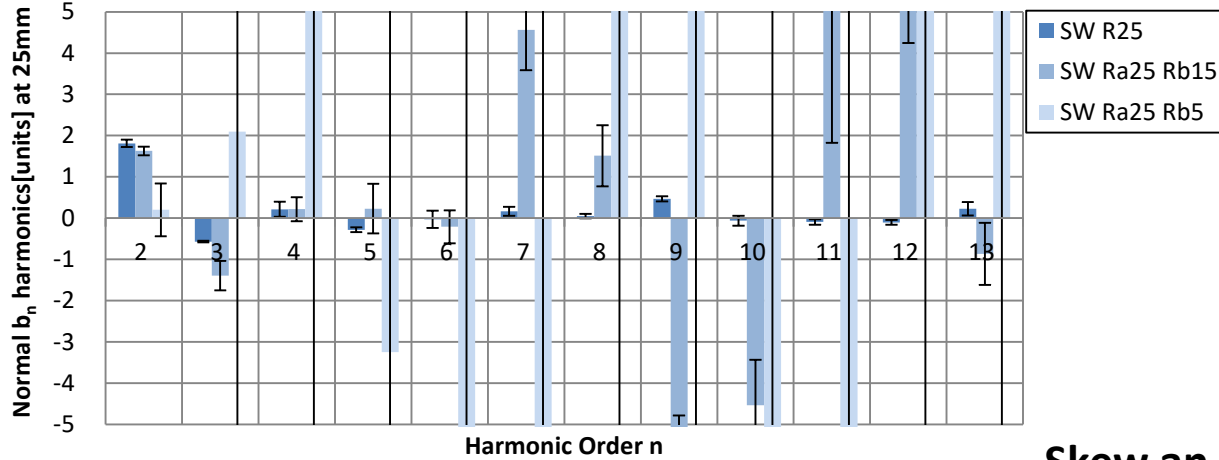
Skew a_n harmonics



HPS Path	B1 (T)
Circle R25	5.178
Ellipse Ra25 Rb15	5.177
Ellipse Ra25 Rb5	5.176

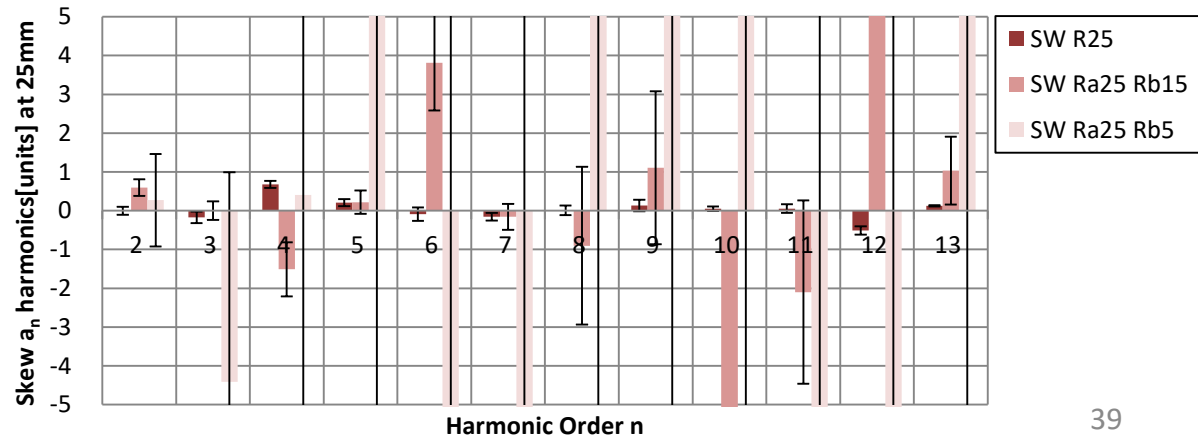
Circle vs Ellipse

Normal b_n harmonics



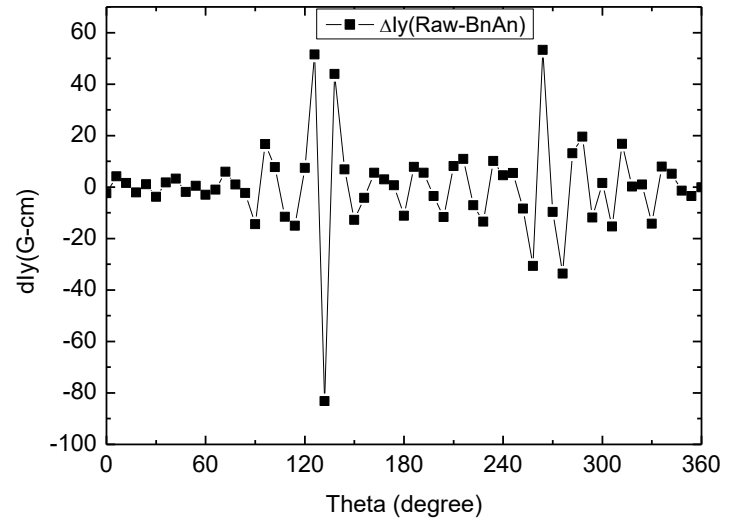
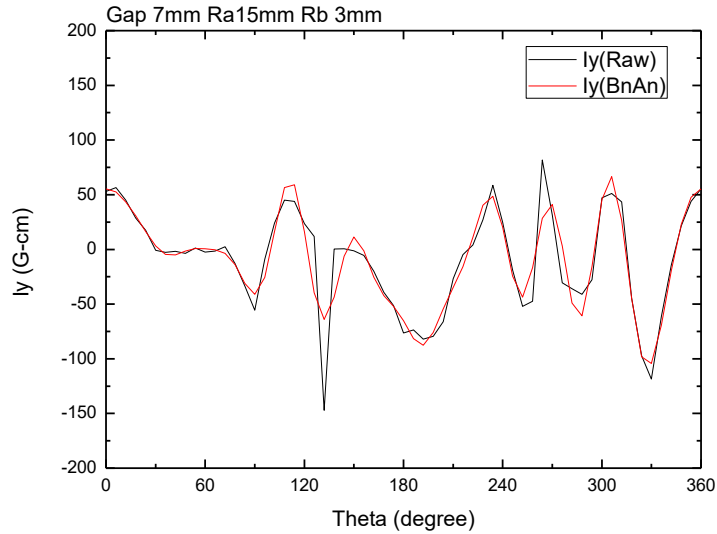
Normalize at long axis radius

Skew a_n harmonics

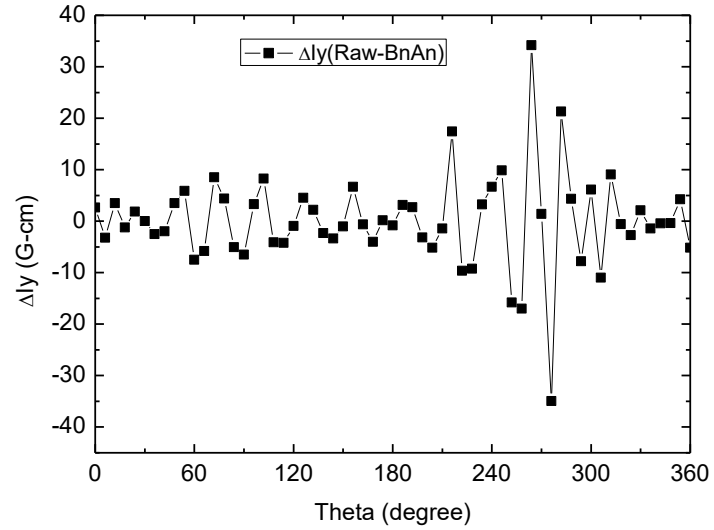
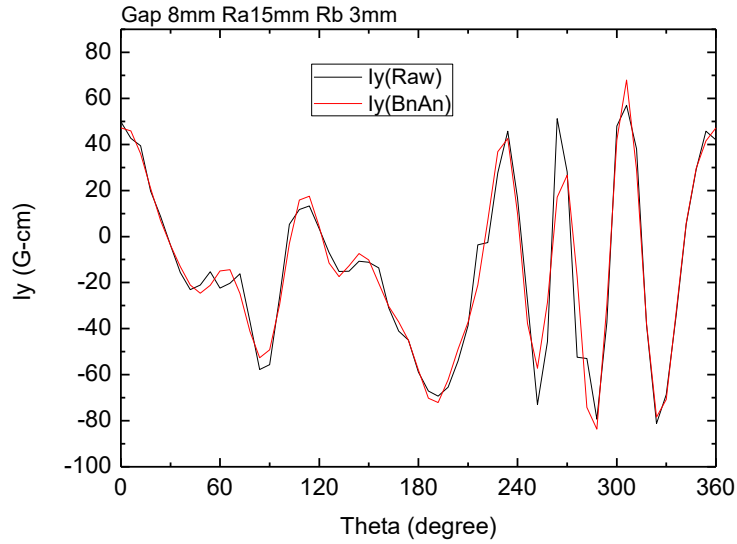


SW Path	B1 (T)
Circle R25	5.179
Ellipse Ra25 Rb15	5.174
Ellipse Ra25 Rb5	5.176

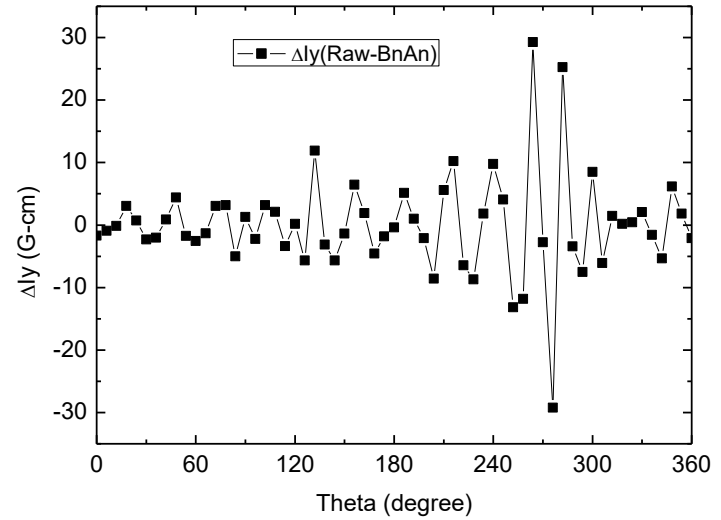
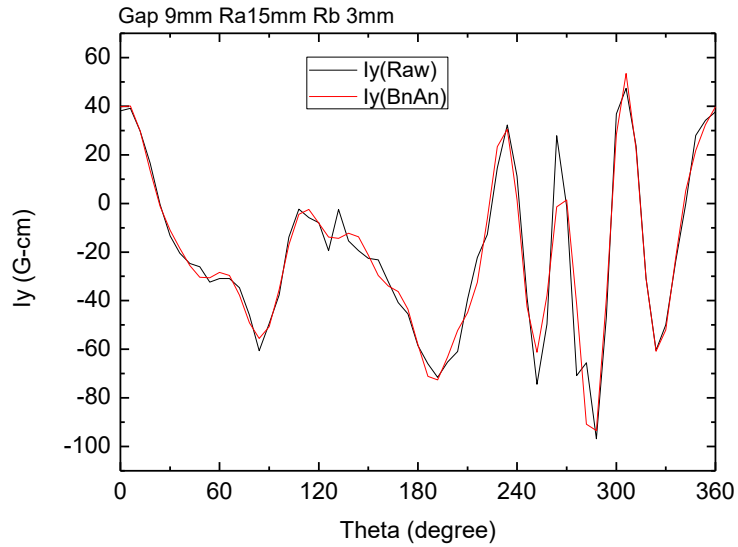
IU24 Gap 7mm



IU24 Gap 8mm



IU24 Gap 9mm



IU24 Gap 10mm

