

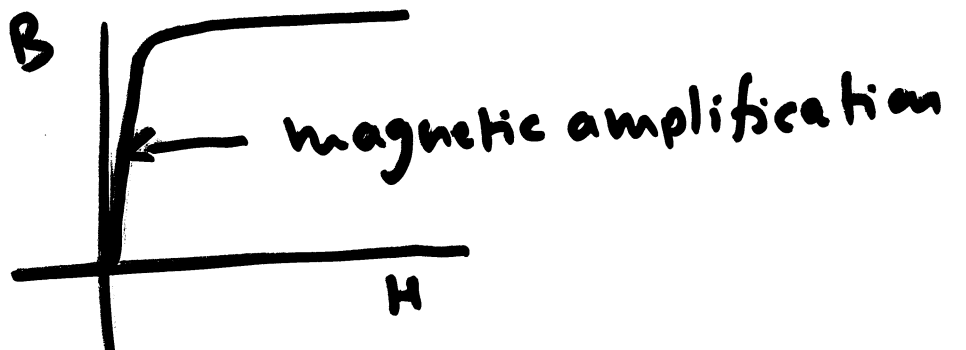
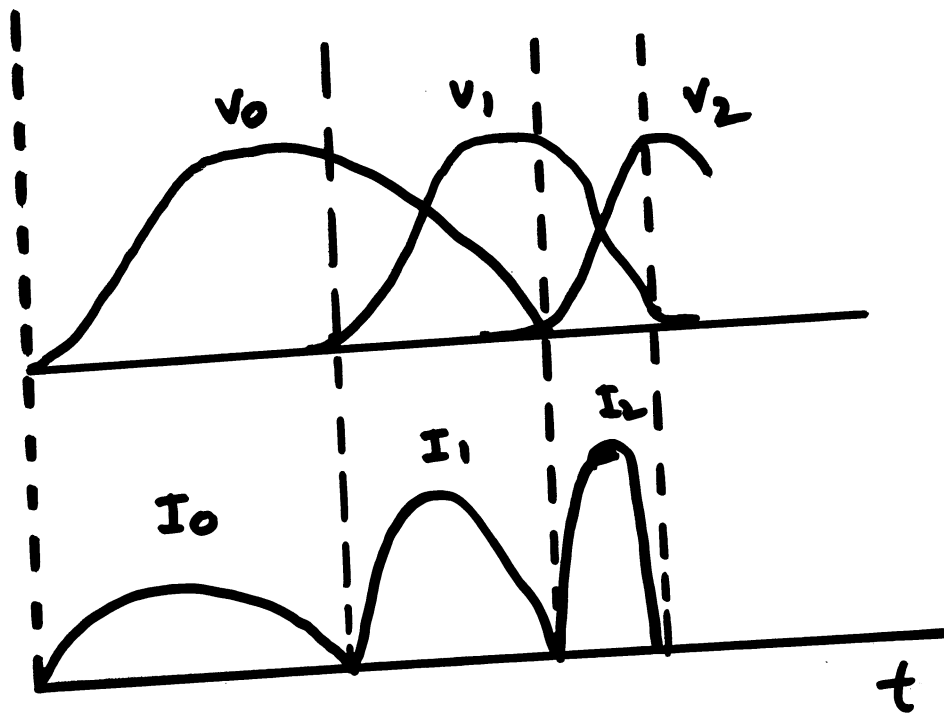
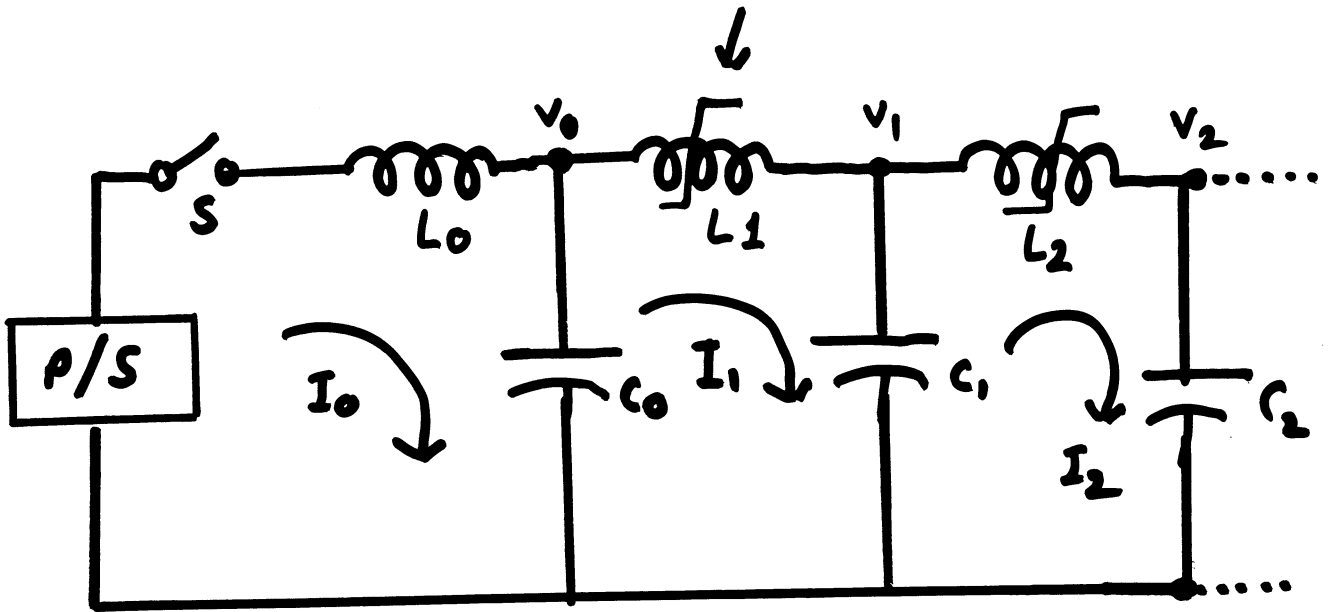
Development
of
Electronic Hysteresigraph for DC
Magnetic Testing of Soft Magnetic
Materials

by

R. S. Shinde , et al
on behalf of Magnetism Group
Centre for Advanced Technology
CAT, INDORE, INDIA

Magnetic Switches:

amorphous core



Brief Background : We have undertaken dev. of Magnetic Pulse Compressors for Pulse P/S to be used in Accel and Laser systems.

- * Initial stages of Magnetic Switches - uses amorphous cores for obtaining pulses $\sim 1 \mu\text{s} \sim 100 \text{ ns}$, due to large ΔB , high pulse current is generated
- * Further, to compress the pulses to the order of 50 ns , we used NiZn ferrite toroids.
- * Therefore, we developed electronic hyst eqpt to measure hyst parameters of magnetic materials.

Electronic Hysteresisgraph

- * An automatic device for DC magnetic testing of soft Magnetic materials

Principle of Device

- * It is based on the classical method, but the Ballistic Galvanometer has been replaced by an electronic Integrator, and a semiconductor switch,
- * Electronic Hysteresis graph method is proposed for determining the dc magnetic materials

Main features of electronics hysteresis graph equipment.

- (a) Ability to trace Magnetic curve keeping induction flux derivative (dB/dt) constant which minimize the error due to the eddy currents in the test specimen.
- (b) The low drift of integrating circuit, which allows tracing Hysteresis loop of specimen in 100 sec.

Instrument Description

The hysteresigraph employs a instrumentation amplifiers, power amplifiers (current), Bistable circuits (timing), electronic integrator, dB/dt control loop & PC base data acquisition system.

The block diagram of the instrument is shown in fig.1

Electronic hysteresis graph instrument consist of

1. B loop : Amplifier and integrator for magnetic induction
2. Magnetizing current loop: Current Amplifier, integrator and Bistable circuit for a perfect symmetry of the hysteresis loop, stability of excitation levels (dB/dt constant)
3. Digital storage oscilloscope: - For tracing of hysteresis loop Accuracy: 1 %
4. ADC: - Computerized data acquisition system software for calculation of magnetic properties of soft magnetic material

Data presentation on PC has accuracy of ADC (12 Bit) H & B ~ 0.1%

Instrument Operation:

* Magnetic test sample: Three windings,

N_p : magnetizing field

N_b : develop voltage proportional to the time derivative of the induction field (dB/dt)

N_c : supplies control loop: \rightarrow Magnetizing current loop - maintaining dB/dt constant.

* Secondary circuit (B. circuit): \rightarrow

Field change gives rise to an induced voltage in N_b , which is integrated drives the Y axis

$$V_o = N_b \frac{\partial \Phi}{\partial t} = N_b A \frac{dB}{dt} \rightarrow B$$

* Magnetization Circuit:

The magnetization current is supplied by the power amplifier which is driven by the integrator. The output of this integrator is the integral of the algebraic

sum of two voltages -

(i) Constant voltage coming from Bistable circuit

(ii) Voltage proportional to the induced voltage in N_b .

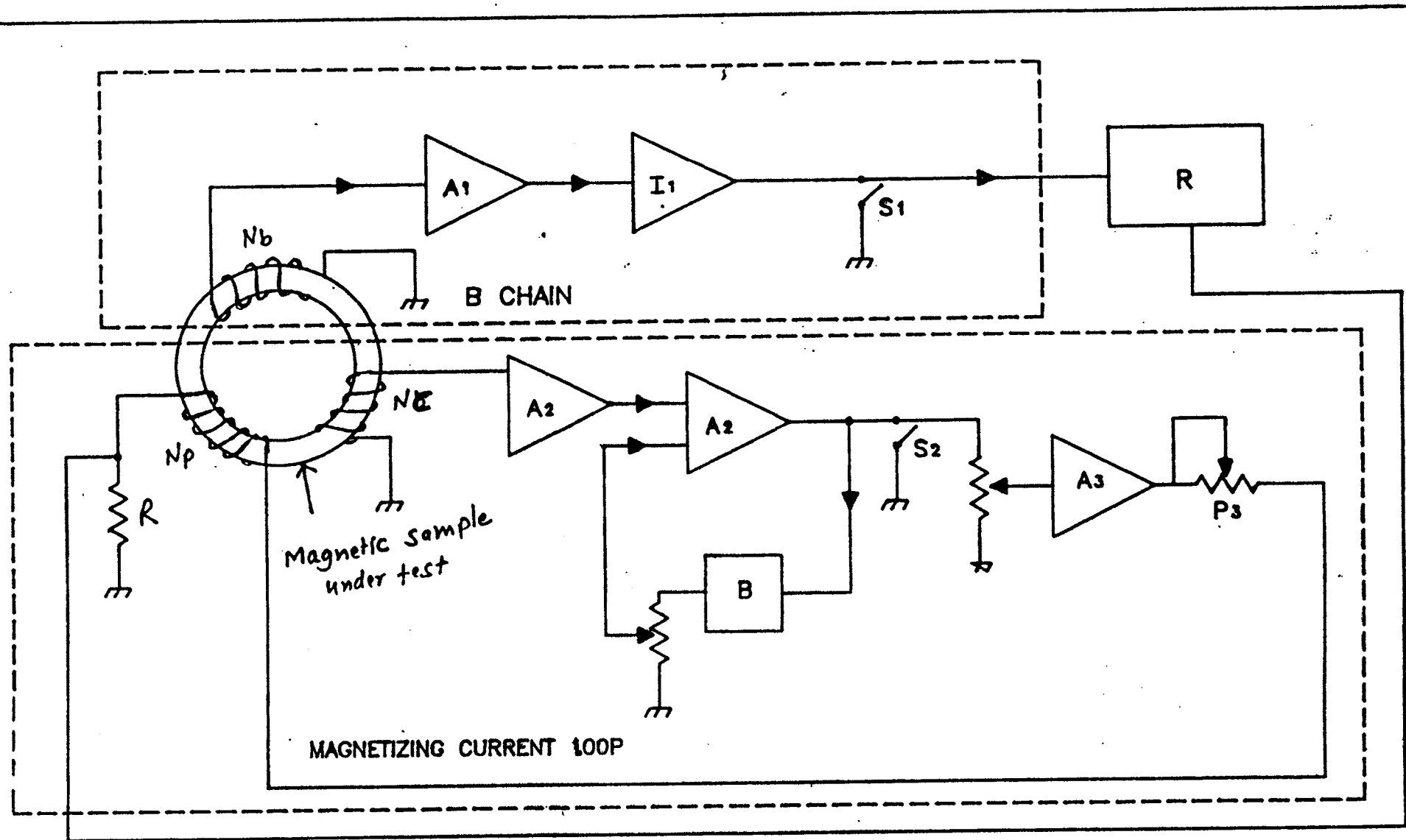
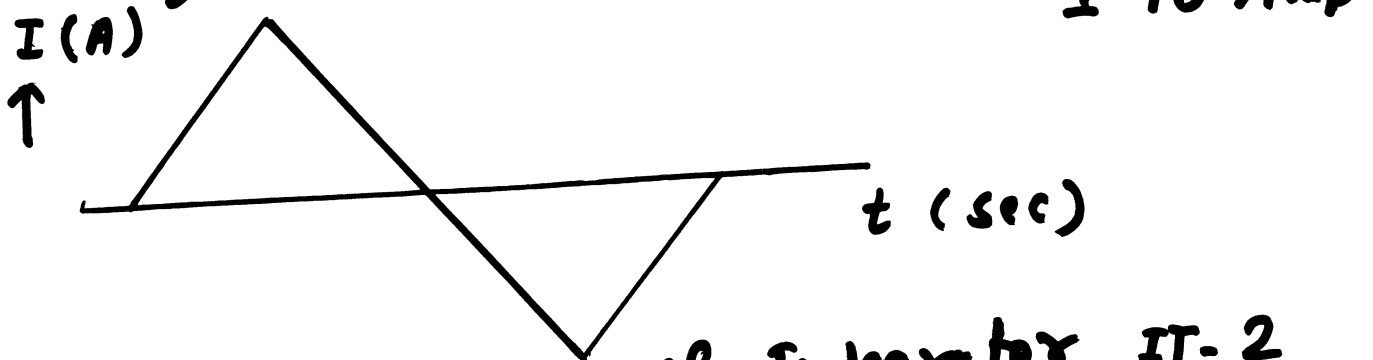


FIG-1 BLOCK DIAGRAM OF THE HYSTERSISGRAPH INSTRUMENT

* Magnetizing current loop: $\frac{dB}{dt}$ constant

- Initially, in the absence of voltage V_c the output of Power Amplifier (A) is a triangular waveform



The output voltage of Integrator IT-2 is the integral of a constant voltage, increases linearly with time. When this voltage reaches a fixed level it switches the bistable circuit, whose polarity is reversed.

Thus the output voltage of Integrator (IT-2) becomes linearly decreasing function of time. When a fixed negative level (-5V) is reached then polarity of Bistable is reversed - again increases with time until a fixed voltage (+5V) and so on.

When the winding N_c is connected to the integrator (IT-2), it controls the rate of change of the magnetizing field maintaining a constant dB/dt .

Actually the gain of IT-2 is very high, the difference between voltages in the inputs A & B of IT-2 vanishes.

Thus, the induced voltage in N_c is constant and so dB/dt .

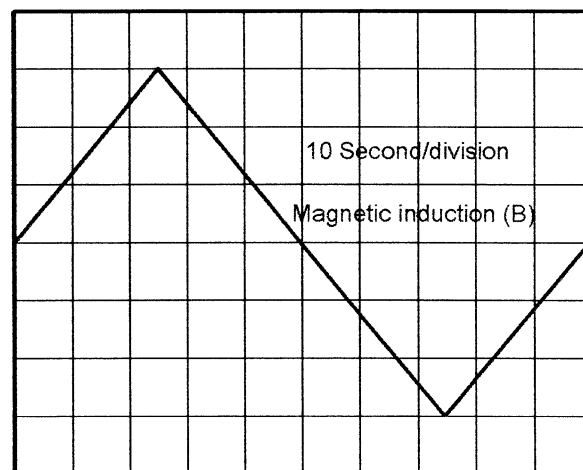
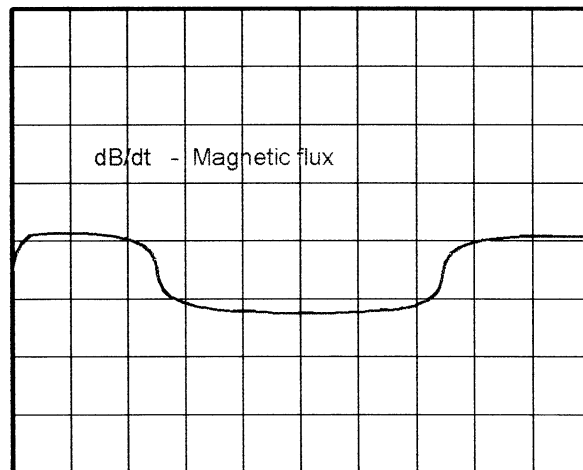
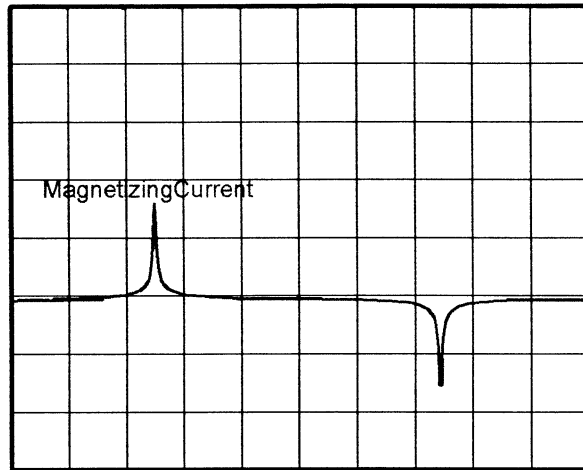


Fig: Waveform showing dB/dt constant during Hysteresis graph

Equipment Components:

1. Integrator
2. Bistable Circuit
3. Power Amplifiers

Integrator: Based on a d.c. amplifier
Small drift & a high
open loop gain

Bistable Circuit: voltage comparator
having two stable states,
each being excited when
its input assumes two
fixed values, which, for
a sym loop must be
equal & opposite.

These states give, at the output of B,
two voltages, which, in order to obtain
the same dB/dt in two halves of the
loop, must be equal & opposite.

Power Amplifiers & Bistable Circuit

: Designed & built by Industries
for CAT, Indore (India)

Measurements :

1. First Magnetization Curve :

Specimen demagnetized : started from saturation point, during demagnetization process I decreased step by step until lowest value of interest (say ~ 150 Gauss). During demagnetization \sim reads integrated signals not current.

set I from power amplifier $\rightarrow \frac{dB}{dt}$

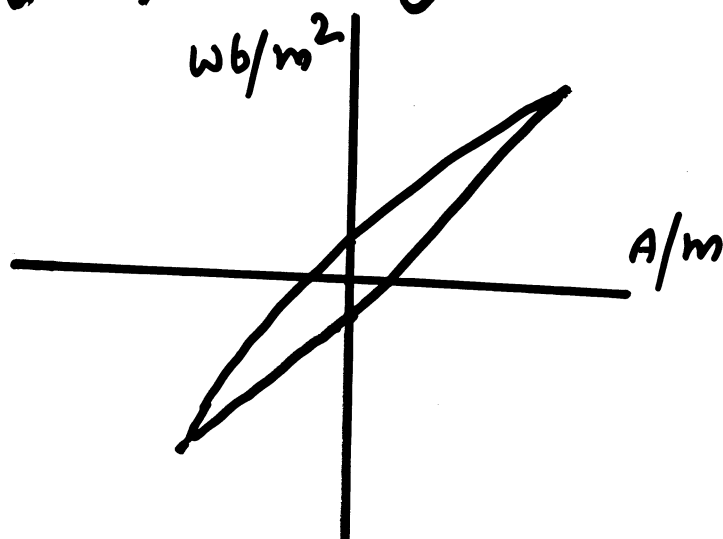
2. Hysteresis Loop

Select Max current to saturate the material. Computer software.

B_s, B_r & H_c

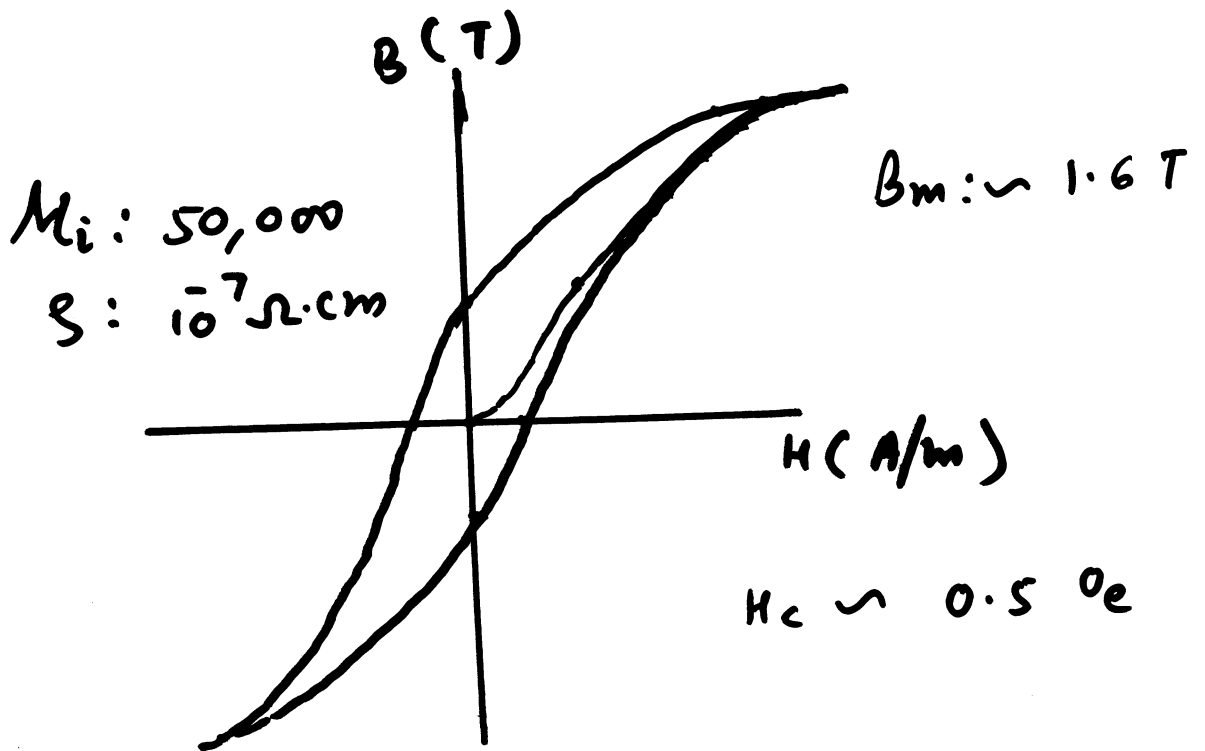
3. Initial Permeability (μ_i)

The specimen - demagnetized. The μ_i obtained by making a small loop



EXPERIMENTAL RESULTS:

Soft magnetic materials: supermalloy, permalloy,
metallic ribbon wound cores
Ni-Fe alloy wound cores, etc.



Hysteresis Loop: supermalloy
(Midhani 78B)

Loop was traced in 3 min.

Accuracy and Sensitivity of Equipment

Accuracies : B & H Scale

- **B accuracy**

Limited by

i) Measurement time: select to avoid error due to eddy currents

- * This can be controlled by maintaining dB/dt constant in hysteresis operation.

- * Reducing rate of change of magnetizing field

ii) Drift of Amplifiers, stability of gain of amplifier & linearity of Integrator

Magnetic samples :

i) Laminated magnetic materials : NiFe wound core
duration of measurement ~ 100 second enough to avoid eddy current error for tracing hysteresis loop.

ii) Metglas- Amorphous ribbons
duration of measurements ~ 4 to 5 minutes is required to trace the hysteresis loop.

$$\mu_{\text{Max}} \sim 100000$$

The overall accuracy for B measurement is about 0.5% obtained

Accuracy and sensitivity

Detail measurements are in process for flux density & coercivity of various, reference materials over a range of different magnetic field strengths.

However, Accuracy of measurement lie between 1% to 0.1% for hysteresis loop parameters (Bs, Br, Hc,)

Test Sample Results

Ref. material sample	Coercivity A/m		Max. Permeability		Saturation flux density Tesla (A/m)	
	Observed CERN	Observed CAT	Observed CERN	Observed CAT	Observed CERN	Observed CAT
1. CERN Steel 54/1125/1	84.77	82.4	4500	4380	2.048	2.033
2. CERN Steel 9268/1	43.2	45	6000	5800	2.017	2.010
3. Ni-Zn-Co Ferrite, 250L	40.0	42	250 NPL	240	0.305 NPL	0.30
4. Decarburized Steel (Raymond Steel)	Measur- ement 257 at CERN	Observed at CAT 262	2200	2140	2.02	2.01

Performance factor

Minimum flux change per second, which can be measured

Performance factor ~ function of the required accuracy and

duration of measurement ~ 100 second

Drift: $0.01 \mu\text{V}$

Maximum flux change, $\Delta\phi = 0.01 \times 10^{-6} \times 100$
 $\sim 1 \times 10^{-6} \text{ web}$

Maximum value of drift – correspond to a flux change of $1 \times 10^{-8} \text{ web/sec}$.

Performance factor: Minimum flux change per second
 $\sim 1 \times 10^{-8} \text{ web/sec}$.

With 0.5% accuracy, PF: $\sim 5 \times 10^{-6} \text{ web/sec}$.
Obtained

Specimen dimension: low carbon steel

50 mm OD \times 45 mm ID \times 100 Ht

Cross sectional area: 25 mm^2

No. of turns: 100

Maximum induction $\sim 2.1 \text{ Web/m}^2$

Flux change during a half cycle is $2.5 \times 10^{-5} \text{ web}$

The error due to the drift during the same time:
 $0.01 \mu\text{v} \times 50 \sim 0.5 \times 10^{-6} \text{ web}$, the error being about
0.1 % (at saturation)

Magnetic Field distribution : →

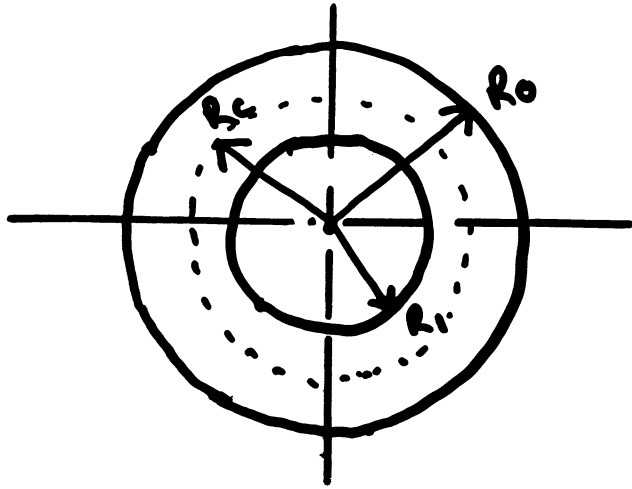


Fig: Ring Specimen

Field H in the ring specimen varies as a function of the radius, its mean value \bar{H} is given by

$$\bar{H} = \frac{1}{R_0 - R_1} \int_{R_1}^{R_0} \frac{NI}{2\pi R} dR = \frac{NI}{2\pi R_c}$$

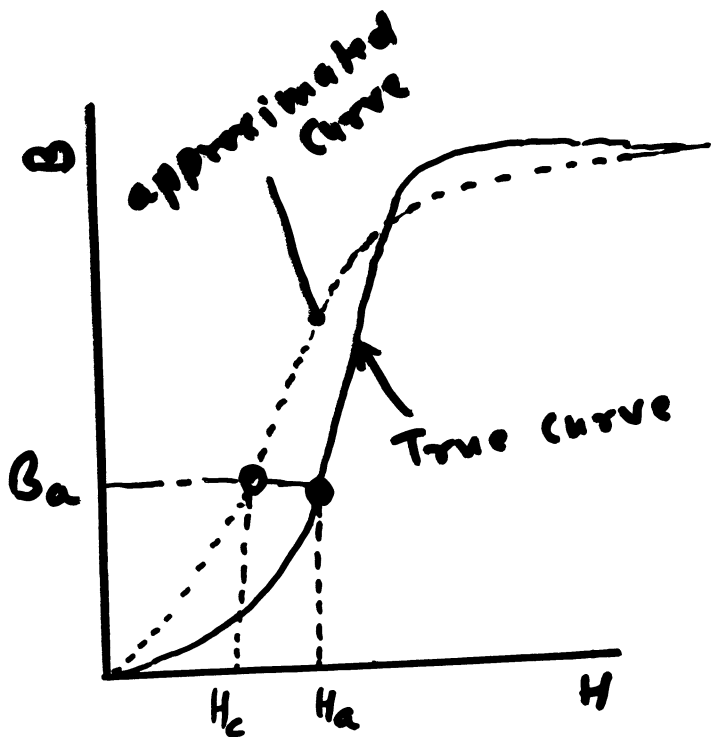
Where $R_c = \frac{R_0 - R_1}{\ln R_0 - \ln R_1}$

Magnetic Flux distribution:

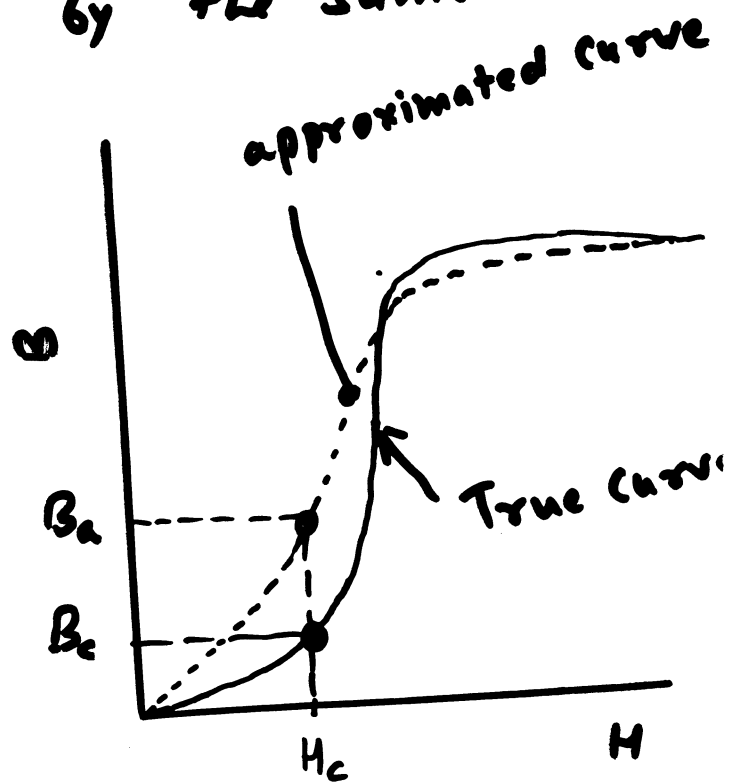
* $B(R)$ can not be measured, but the average flux density, $B(a)$ can be measured using a search coil.

* The average values of the magnetizing field and of the flux density will not correspond to each other

→ as the distribution of H and B are not described by the same fn.



Error in H



Error in B

Error in H : Magnetic field H_c on the mean radius $R_c = \frac{R_o + R_i}{2}$ is used

Actually we should measure H_a on mean magnetic path corresponding to B_a .

Error in B : Measure B_a corresponding to H_c .
Flux density B on the centre radius $R_c = \frac{R_o + R_i}{2}$
Actually we should measure B_c .